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A MULTIVARIATE AUTOREGRESSIVE FORECAST MODEL

FOR SHORT-TERM PREDICTIONS

Ву

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Under Contract DAAG29-72-0-0100

Contract Monitor: Bruce T. Miers

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Data from 3 years (1972-1974) of synoptic observations collected at seven German stations were used to determine multivariate autoregressive (MVAR) models to make short-term forecasts (3 to 12 hours) for six atmospheric variables (temperature, u-wind, v-wind, visibility, ceiling height, and height of first cloud layer). So that certain tactical constraints could be met, the order and number of predictor variables used by the MVAR models were limited. To emphasize the variance of low ceiling and visibility situations, a variable transformation was

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## 20. ABSTRACT (cont)

performed upon the observations of visibility and the cloud height variables. The best forecasts were obtained when six seven-parameter MVAR models were used. Each model produces a forecast for a particular variable, using the observations at the seven stations as parameters. The variables that can be forecast best are temperature and the u- and v-components of the wind with about 95, 75, and 60 percent of the variance, respectively, explained by the model. From 45 to 70 percent of the variance is explained by the model for visibility while from 30 to 60 percent is explained for the cloud height variables. Finally, data from observations collected in 1976 were used in testing the MVAR models, and the error statistics from these actual forecasts agreed with theory.

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# TABLE OF CONTENTS

# Section

1	Intro	oduction	į
2	Multi	ivariate Autoregressive Forecast Model	,
3	Preli	iminary Data Analysis	1.3
4	App1i	ication and Results	18
5	Concl	usions	29
6	Refer	rences	31
APPENDIX	( A.	COVARIANCE AND COEFFICIENT MATRICES FOR THE SIX VARIABLE-AT-A-TIME MVAR MODELS	22
APPENDIX	С В.	PROGRAM LISTINGS AND FLOWCHART OF ANALYSIS PROCEDURES	4.

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#### 1. Introduction

The purpose of this research is to develop a multivariate autoregressive (MVAR) climatological model to be used for short-term forecasting (3-12 hours) of various atmospheric variables over a limited area in a tactical situation. The atmospheric variables to be forecast are temperature, visibility, ceiling height, height of the first cloud layer, and the u- and v-components of the wind. The tactical situation facing the forecaster is this: all of his communications are cut off and he must, using only a small computer with limited storage area, make 3-hourly forecasts of the aforementioned variables out to 12 hours over an area on the order of 100 km square. Using an MVAR model the forecaster can not only make the necessary forecasts, but confidence intervals about the forecast values can also be computed to aid in any decision-making processes based on these forecasts.

In the next section a theoretical description of an MVAR forecast model is presented. In such a model the forecast value of a variable (predictand) is assumed to be a function of present and past observations of that variable as well as other predictor variables. The relationships between the predictand and the predictors are carried within the coefficient matrices of the model which are determined from the past history of observations. Embedded within these coefficient matrices will be the effects of complex terrain upon the inter-relationships among the predictand and predictors.

The data used in this study consisted of five years of 3-hourly observations of the six variables to be predicted as well as one predictor variable, the dewpoint temperature, for the following north German stations: Hannover, Bremen, Braunschweig, Boizenburg, Magdeburg, Weissen, and Wernigerode. In Section 3 the preliminary data analysis is described in which the distribution and various statistical properties of the variables were determined. From

the results of this analysis it was decided that the cloud height of ibility variables be transformed in such a way that the variance productions low visibility and ceiling conditions be emphasized so that a conditions could be better forecast.

determined using the first three years of data (1972-1974). With the data storage available to the forecaster it was as the final models could only utilize values of the predictors for the period preceding the forecast time. It was found that under the take constraints the best forecasts could be obtained using six 7-parameter.

MVAR models. Each model produces a forecast for a particular variable and the observations at the seven stations as parameters. The variable and one can theoretically expect to forecast best are temperature and the variance, respectively, explained by the model. The percent variance consequence to explain ranges from about 45 to 70 for visibility and from about 30 to 60 for the cloud height variables. Using the data from 1976 the Models were tested and the error statistics from these actual forecasts were found to agree quite well with theory.

## 2. Multivariate Autoregressive Forecast Model

In this section the theory behind a multivariate autoregressive (MVAR) forecast model will be outlined. Suppose that one has collected m time series consisting of n observations each for m different variables. Further assume that the value of the sample mean has been subtracted from each of these observations. Using these observations one would like to develop a forecast model such that future values for  $m_1 \leq m$  of these variables may be predicted, given the present and a certain number of past values of these variables. For a particular time i the observations for the m variables are denoted by the m-dimensional column vector,  $X_1$ , where the first  $m_1$  elements of  $X_1$  belong to the  $m_1$  time series to be predicted while the last  $m_1$  belong to those series to be used to aid in the forecast. The p-th order MVAR model is:

$$X_i + A_1 X_{i-1} + \dots + A_p X_{i-p} = Z_i$$
 (1)

where the A's are mxm coefficient matrices and  $Z_i$  is an m-dimensional white noise column vector. Such a model would use the present observations  $(X_{i-1})$  and p-1 past observations in order to predict the values of the variables one interval in the future  $(X_i)$ . The variance of the white noise process  $(Z_i)$  represents the one-step prediction error variance of forecasts made with this model. Two things must be determined, using the collection of n observation vectors, before an MVAR forecast model can be developed. First, the proper order model must be selected and then the coefficient matrices for that order model must be computed.

The procedure outlined in this section is the multivariate generalization given by Whittle (1963) of the recursive method developed by Durbin (1960) for the fitting of univariate autoregressive models of successively increasing order. Except for the inclusion of the Akaike FPE criterion (Akaike, 1971), it is identical to that presented by Jones (1964). The Akaike FPE parameter is an estimator of the one-step prediction error of the MVAR process. The use of the FPE criterion permits one to find the order model with the smallest one-step prediction error. The analysis procedure can be described simply: first, L + 1 MVAR models whose order successively increase from zero to L are fitted to the n m-dimensional observation vectors using the recursive method to be detailed below; for each order model a value of the Akaike FPE parameter is computed, and finally, an MVAR model whose order is that for which the minimum FPE was found is fitted to the data using the same recursive method. This is the model that one would use for prediction.

The first step in the analysis method is the calculation of the lag sums  $\ensuremath{\mathsf{L}}$ 

$$G_{p} = \sum_{i=p+1}^{n} X_{i}X_{i-p}^{-}, p=0,1,2,...,L,$$
 $G_{-p} = G_{p}^{-}$ 

where  $G_p$  denotes the transpose of the m x m matrix  $G_p$ . In the following equations the p-th order residual matrices for the forward and backward autoregressions are denoted by  $S_p$  and  $\overline{S}_p$ , respectively. The k-th coefficient matrices for the p-th order forward and backward autoregressions are denoted by  $A_k^p$  and  $\overline{A}_k^p$ , respectively. The determinant of the  $m_1$  x  $m_1$  submatrix in the upper left-hand corner of  $S_p$  is denoted by  $S_p, m_1$ .

$$S_0 = \overline{S}_0 = G_0$$
 $A_1^1 = -G_1 \overline{S}_0^{-1}$ 
 $\overline{A}_1^1 = -G_{-1}S_0^{-1}$ 
 $FPE_0 = (\frac{n+1}{n-1})^m 1 |S_0, m_1|$ .

For p = 1, 2, ..., L-1,

$$\begin{split} S_p &= G_0 + A_1^p G_{-1} + \dots + A_p^p G_{-p} \\ \overline{S}_p &= G_0 + \overline{A}_1^p G_1 + \dots + \overline{A}_p^p G_p \\ FPE_p &= (\frac{n+pm+1}{n-pm-1})^m 1 \mid S_p, m_1 \mid \\ A_{p+1}^{p+1} &= -(G_{p+1} + A_1^p G_p + \dots + A_p^p G_1) \overline{S}_p^{-1} \\ \overline{A}_{p+1}^{p+1} &= -(G_{-p-1} + \overline{A}_1^p G_{-p} + \dots + \overline{A}_p^p G_{-1}) S_p^{-1} \\ \overline{A}_{p+1}^{p+1} &= -(G_{-p+1} + \overline{A}_1^p G_{-p} + \dots + \overline{A}_p^p G_{-1}) S_p^{-1} \\ A_k^{p+1} &= A_k^p + A_{p+1}^{p+1} \overline{A}_{p+1-k}^p \\ \overline{A}_k^{p+1} &= \overline{A}_k^p + \overline{A}_{p+1}^{p+1} A_{p+1-k}^p \\ \hline A_k^{p+1} &= \overline{A}_k^p + \overline{A}_{p+1}^{p+1} A_{p+1-k}^p \end{split}$$

Finally,

$$S_L = G_O + A_1^L G_{-1} + ... + A_L^L G_{-L}$$
  
 $FPE_L = (\frac{n+Lm+1}{n-Lm-1})^m 1 | S_L, m_1|.$ 

Thus, if one had found that  $FPE_k$  had been a minimum and had fitted at k-th order MVAR model to the data, the prediction for  $X_i$  given  $X_{i-1}, \ldots, X_{i-k}$  would be

$$X_{i} = -A_{1}^{k} X_{i-1} - A_{2}^{k} X_{i-2} - \dots - A_{k}^{k} X_{i-k}$$
 (2)

At this point the values of the sample means for the variables to be predicted would be added back to the  $X_i$  vector to give the final prediction value for each variable.

Finally, one can determine the quality of the predictions from such a model by computing the prediction error covariance matrices. For a k-th order model the one-step prediction error covariance matrix is

$$V_k^1 = \frac{1}{n-mk} S_k .$$

Successive predictions can be made—using—(2) by merely replacing observativalues by predictions as one steps further into the future. The following recursion is used to find the j-step prediction error covariance matrix,  $V^{j}$ , when using repeated predictions:

$$B_1 = -A_1$$
 
$$B_j = -(A_j + B_1 A_{j-1} + \dots + B_{j-1} A_1)$$
 and 
$$V^j = V^{j-1} + B_{j-1} V^1 B_{j-1}.$$

Once this matrix has been obtained, its main diagonal consists of the error variances for the variables to be predicted. These can then be used to determine confidence intervals to be placed about the forecast values.

## 3. Preliminary Data Analysis

Before an attempt was made to determine any MVAR models, a preliminary data analysis was performed using the 3-hourly observations

(00Z, 03Z, etc.) collected during 1972-1975 for the following stations:

Hannover, Bremen, Braunschweig, Boizenburg, Magdeburg, Weissen, and

Wernigerode. First, the distributions of the six variables as the predicted (temperature, u- and v-components of the wind, visibility, ceiling height, and height of the first cloud layer) were determined. In Figure 1 the distribution of the 1972-1975 temperature and u-wind observations for Wernigerode are displayed with their sample means denoted by a star. The distributions shown here are typical of the temperature and u- and v-wind observations for all seven stations used in this study. As can be seen in Figure 1, these variables appear to be quite normally distributed.

On the other hand the distributions found for visibility and the cloud height variables were far from normal. In Figure 2a the distribution found for the visibilities observed at Wernigerode is shown. This distribution, which is typical of those found for the visibility and cloud height variables at all seven stations, is roughly rectangular with a sample mean of just over 9 km. However, since an MVAR model is designed to predict deviations of the variables about their sample means and since for these three variables the sample means are much larger than the low visibility and low ceiling situations that one would like to be able to predict, the following transformations were performed upon these variables in order to emphasize the variance of the low visibility (ceiling) situations:

$$V2 = \exp(-V1/2000) \tag{3}$$

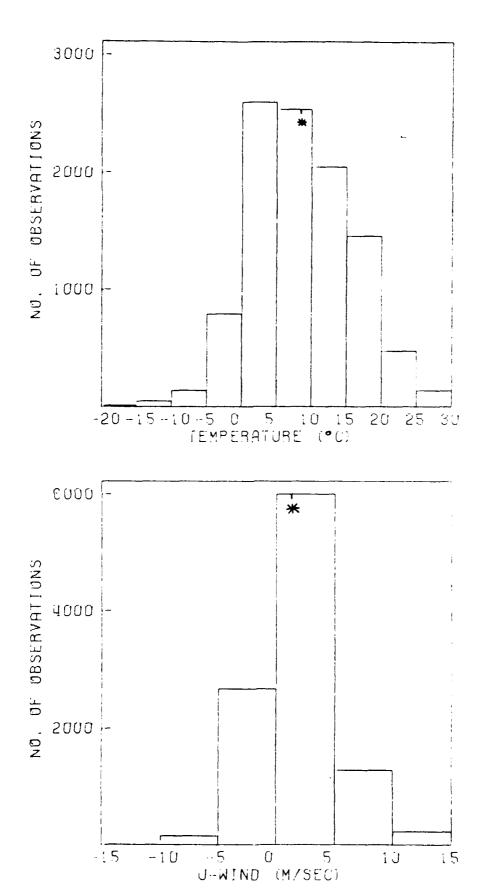


Figure 1. Distribution of 1972-1975 temperature and u-wind observations for Wernigerode.

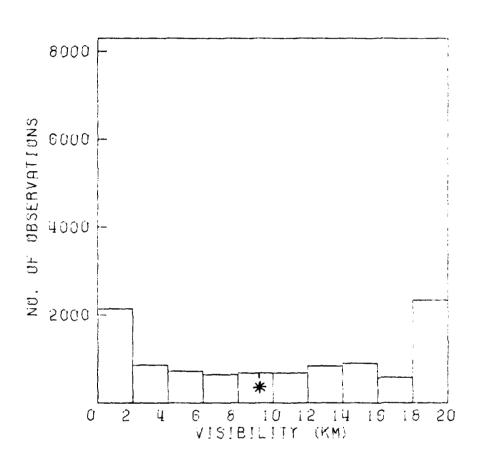


Figure 2a. Distribution of 1972-1975 visibility observations for Wernigerode.

$$C2 = \exp(-C1/1000),$$

(4)

where V1 and C1 are the observed visibility and cloud height, respectively. in meters. In Figure 2b we can see the effect of this transformation upon the visibility distribution for Wernigerode. The sample mean of the transformed variable now represents a visibility of only 2.4 km. Furthermore, an observation of visibility less than 1 km will contribute more to the variance than an observation of unlimited visibility since its deviation from the sample mean will be larger. By expanding the scale for low visibilities and decreasing the scale for high visibilities, this transformation permits more precise forecasts of the poor visibility situations.

Next, monthly and hourly means were computed for all variables at all stations using the 1972-1975 observations. Table 1 summarizes the

Table 1. Variance explained by monthly and hourly means for Hannover (1972-1975).

Variable	Total Variance	Variance Monthly Means			Percent
First Cloud Layer Ht.*	.0791	.0052	6.6	.0036	4.6
Ceiling Ht.*	.0843	.0070	8.3	.0028	3.3
Temperature	53.49	32.13	60.1	4.70	8.8
Visibility*	.0331	.0021	6.3	.0013	3.9
u-wind	13.63	.79	5.8	.062	0.5
v-wind	6.08	.52	16.4	.32	0.5

\* Indicates transformed variable.

results of these computations for Hannover, which again are typical of those found for the other stations. We can see that with the exception of monthly averages for temperature, only a small percent of the total variance for the six variables is explained by the annual and diurnal cycles.

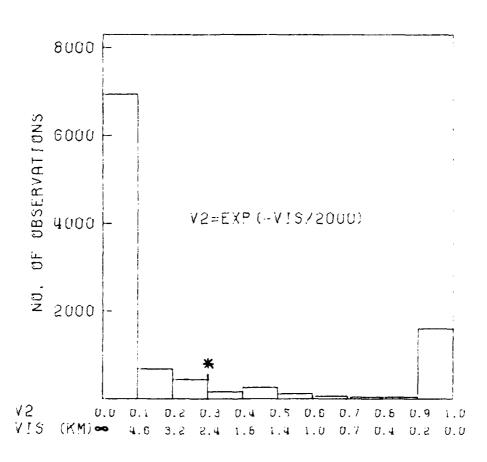


Figure 2b. Distribution of transformed 1972-1975 visibility observations for Wernigerod.

Typically, about 60 percent of the temperature variance is explained by the annual cycle. Plots of the hourly and monthly means for Hannover are displayed in Figure 3. We can see that the amplitude of the annual wave is about 8°C while that of the diurnal wave is about 3°C. Since all seven stations display this pronounced annual wave for temperature and it explains a significant amount of the variance, its effect will be removed from the temperature data along with that of the diurnal cycle and the sample mean before any MVAR models are determined for that variable. One must be careful when attempting to fit an MVAR model to data which are highly correlated since unstable processes can be produced. In any case, it is the deviations about these very regular cycles that we are interested in forecasting, and, thus it is these deviations which we will attempt to model.

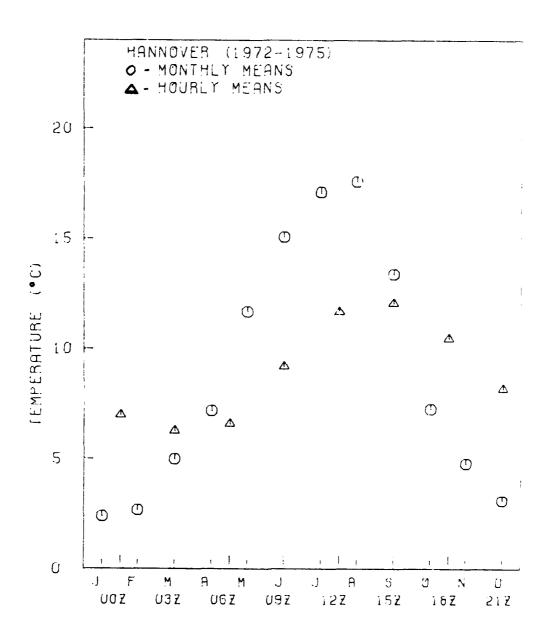


Figure 3. Monthly and hourly means computed from 1972-1975 Hannover temperatures.

#### 4. Application and Results

Using observations collected during 1972-1974 the MVAR modeling process described in Section 2 was applied in several different ways in order to determine the best forecasting technique. Given the tactical constraint of limited computer size and storage, we will only consider MVAR forecast models of order nine or less. Thus, only a one day history of observations of the predictor variables need be stored at a time. This tactical consideration also limits the number of variables to be used by the MVAR models (not only those to be predicted but also those to aid in the prediction). For example, if an MVAR model were developed which used all of the observed variables for all stations, then it would possess 49 variables. If the model were of order nine, then nine 49 x 49 coefficient matrices would have to be stored and used in the forecast computations along with nine 49 x 1 observational vectors from the past 24 hours. This would require almost 100 K bytes of storage and a comparably large number of computations required to make the forecasts. On the other hand, a model of order nine with only seven variables would require about 50 times less space and computation time.

The first type of MVAR model to be tested used the six variables to be predicted (temperature, u- and v-wind components, visibility, ceiling height, and height of the first cloud layer) along with the dew-point temperature for one station at a time. The analysis procedure outlined in Section 2 was applied using the 1972-1974 observations to calculate the lag sum matrices. The model order was restricted to be no greater than nine and this maximum was chosen in every case except for Braunschweig where an eighth order model possessed the smallest Akaike FPE parameter. The

7 x 7 coefficient matrices for each resulting station model were determined along with estimates of the one-step prediction error variance for the six variables to be forecast. We will use these estimates in order to determine the quality of the various MVAR forecast models tested here. Table 2 summarizes the results for the 7 station models. We can see that using such a

Table 2. Estimates of one-step prediction error variance and percent variance explained (in parenthesis) for the station MVAR models determined from 1972-1974 observations.

Station		Height of 1st Cloud Layer*	Ceiling Height*	Temperature	<u>Visibility</u> *	u-wind	v-wind
Hannover	9	.0374 (54.7)	.0436 (48.6)	2.55 (94.8)	.0164 (52.2)	2.96 (78.8)	2.40 (63.0)
Bremen	9	.0367 (52.8)	.0436 (45.5)	2.93 (93.8)	.0194 (42.4)	3.31 (78.4)	2.99 (67.3)
Boizenburg	9	.0181 (32.2)	.0308 (35.0)	3.75 (92.4)	.0252 (46.8)	4.78 (63.9)	
Braunschweig	8	.0296 (53.2)	.0333 (49.8)	3.12 (92.7)	.0112 (55.0)	2.82 (75.9)	2.46 (59.1)
Magdeburg	9	.0260 (36.3)	.0314 (38.8)	3.58 (93.3)	.1400 (66.7)	3.01 (72.1)	3.17 (52.0)
Wernigerode	9	.0223 (38.4)	.0264 (42.5)	3.9 (92.1)	.0332 (64.6)	3.97 (67.5)	4.16 (46.0)
Weissen	9	.0360 (33.1)	.0391 (38.8)	4.15 (92.4)	.0186 (50.4)	5.01 (67.5)	3.06 (52.9)
*Indicates	transf	ormed varia	able.				

model we can best forecast temperatures (from 92.1 to 94.8 percent variance explained) and are least able to forecast the height of the first cloud layer (from 32.2 to 54.7 percent variance explained). One can roughly expect to explain 40%, 55%, 55%, and 70% of the variance for ceiling height, visibility, v-wind, and u-wind, respectively.

The next type of MVAR model to be investigated utilized the observations for a particular variable at all seven stations. Again the model order was restricted to nine or less and the MVAR analysis procedure was applied to the 1972-1974 observations for the six different variables to be forecast. In Table 3 the estimates of the one-step prediction error variance and the percent variance explained for the 6 variable models are displayed. In this case, as discussed in Section 3, the monthly and hourly

Table 3. Estimates of one-step prediction error variance and percent variance explained (in parenthesis) for the variable MVAR models determined from 1972-1974 observations.

Variable	Model Order	Hannover	Bremen	Boizenburg	Braunschweig	Magdeburg	<u>Wernigerod</u>	e Weissen
Height of 1st Cloud Layer*	9	.0359 (56.5)	.0369 (52.5)	.0183 (31.5)	.0261 (58.7)	.0244 (40.2)	.0224 (38.1)	.0339 (37.0)
Ceiling Height *	9	.0419 (50.6)	.0440 (45.0)	.0298 (37.1)	.0293 (55.9)	.0282 (45.0)	.0263 (42.7)	.0367 (42.6)
Tempera- ture	9		2.34 (95.0)	2.63 (94.7)	2.02 (95.3)	2.35 (95.6)	2.82 (94.3)	3.19 (94.1)
Visi- bility*	9	.0157 (54.2)	.0187 (44.5)	.0241 (49.2)	.0097 (61.0)	.0132 (68.6)	.0335 (64.3)	.0178 (52.5)
u-wind	9	2.51 (82.0)	3.18 (79.2)	3.85 (70.8)	2.28 (80.5)	2.33 (78.4)	3.66 (70.0)	3.88 (74.8)
v-wind	9	2.00 (69.1)	3.08 (66.3)	2.99 (55.6)	2.03 (66.3)	2.51 (62.0)	3.72 (51.7)	2.48 (61.8)
* Indic	ates ti	ransformed	d variat	ole.				

means were removed along with the sample means for the temperature observations.

A comparison of Tables 2 and 3 indicates that in almost every case the percent variance explained by the variable-at-a-time MVAR models is greater than that for the station-at-a-time models. The greatest improvement is noted for the

v-wind predictions where the percent variance explained is increased by as much as 10%. For the variable-at-a-time models we can expect to explain approximately 95%, 75%, 60%, 55%, 45%, and 45% of the variance, respectively, for temperature, u-wind, v-wind, visibility, ceiling height, and height of the first cloud layer.

For the first two types of MVAR models tested here the model order was limited. However, for both types, MVAR models were determined in which the maximum order permitted was 30. In these cases MVAR models whose order ranged from 25 to 30 were found to possess the minimum value of the Akaike FPE parameter. In every case though the reduction of the one-step prediction error variance over that of the ninth order models was negligible. Thus, the limitation of the model size required by the tactical situation has no detrimental effect upon the quality of the forecast models produced.

A final MVAR model was examined in which the number of variables was 21, consisting of the aforementioned seven variables for the stations, Hannover, Bremen, and Braunschweig. Again the model order was limited to nine or less and a ninth order model was chosen by the analysis procedure. Table 4 summarizes the results for this particular model.

Table 4. Estimates of one-step prediction error variance and percent variance explained (in parenthesis) for the three-station MVAR model determined from 1972-1974 observations.

Station	Height of 1st Cloud Layer*	Ceiling Height*	Temperature	Visibility*	u-wind	v-wind
Hannover	.0341	.0391	2.10	.0152	2.46	1.97
	(58.7)	(53.9)	(94.7)	(55.7)	(82.3)	(69.6)
Bremen	.0348	.0416	2.31	.0182	2.97	2.87
	(55.2)	(47.9)	(95.1)	(46.0)	(80.6)	(68.6)
Braunschweig	.0248	.0282	2.19	.0098	2. <b>24</b>	1.98
	(60.8)	(57.5)	(94.9)	(60.6)	(80.8)	(67.1)

'Indicates transformed variable.

Comparing Table 4 with Table 3 one can see that this 21-variable model is only slightly better than the three respective 7-variable models. Therefore, since the variable-at-a-time models can be run using about one-tenth the computer space and time and since there is negligible improvement to be gained from the larger model, they have been chosen as the best MVAR forecast model to be used for short-range predictions in a tactical situation.

We have seen in this section how well, based on the MVAR theory described in Section 2, we can expect to forecast the six meteorological variables of interest in this study. Using the six variable-at-a-time models, whose expected performances are outlined in Table 3, and observations collected during 1976, a number of MVAR forecasts were made and compared with the observations valid at the forecast time. Assuming that the MVAR forecast models are unbiased, theoretical estimates of the root mean square errors (RMSE's) for the one-step through four-step predictions are obtained by simply taking the square root of the one-step through four-step prediction error variances. These theoretical RMSE's are then compared with the actual RMSE's computed from 3-, 6-, 9-, and 12-hour forecasts made using the six MVAR models (developed using 1972-1974 data) upon 1976 observations.

Tables 5 and 6 display the results of 48 MVAR forecasts using the ninth order variable-at-a-time models for the transformed variables height of the first cloud layer and ceiling height, respectively. We can see in Table 5 that in virtually every case the RMSE's computed from the actual MVAR forecasts were smaller than those expected from theory and in no case were they larger. The RMSE's determined from the ceiling height forecasts shown in Table 6 agree quite closely with their theoretical counterparts for four stations (Hannover, Bremen, Braunschweig, and Weissen) and are

Table 5. Comparison of theoretical forecast RMSE's (T) with those computed from actual MVAR forecasts (C) using 1976 transformed height of first cloud layer data.

			RMSE's						
Station	No. of Forecasts	3-hour C	FCST	6-hour	FCST T	9-hour	FCST T	12-hou	ır FCST T
Hannover	48	0.12	0.19	0.18	0.23	0.19	0.25	0.20	0.26
Bremen	48	0.11	0.19	0.16	0.23	0.17	0.25	0.20	0.26
Boizenburg	48	0.10	0.14	0.11	0.15	0.12	0.15	0.12	0.15
Braunschwe	ig 48	0.13	0.16	0.14	0.19	0.20	0.21	0.17	0.22
Madgeburg	48	0.09	0.16	0.15	0.17	0.11	0.18	0.14	C.19
Wernigerod	e <b>4</b> 8	0.08	0.15	0.10	0.16	0.10	0.17	0.09	0.19
Weissen	48	0.17	0.18	0.20	0.20	0.21	0.21	0.22	0.22

Table 6. Comparison of theoretical forecast RMSE's (T) with those computed from actual MVAR forecasts (C) using 1976 transformed ceiling height data.

		RMSE's							
Station	No. of Forecasts	3-hour C	FCST T	6-hour	r FCST	9-hour C	FCST T	12-hou C	r FCST
Hannover	48	0.20	0.20	0.24	0.24	0.28	0.25	0.25	0.27
Bremen	48	0.22	0.21	0.26	0.24	0.27	0.25	0.28	0.27
Boizenburg	48	0.11	0.17	0.12	0.19	0.13	0.20	0.13	0.21
Braunschwe	ig 48	0.19	0.17	0.18	0.20	0.26	0.22	0.20	0.23
Magdeburg	48	0.10	0.17	0.16	0.19	0.12	0.20	0.15	0.21
Wernigerode	48	0.08	0.16	0.10	0.18	0.10	0.19	0.10	0.20
Weissen	48	C 18	0.19	0.20	0.21	0.21	0.22	0.23	0.23

consistently smaller for the other three stations. The results for 46 MVAR forecasts for the third transformed variable, visibility, are shown in

Table 7. With the exception of those found for Boizenburg, the RMSE[s] computed from the forecasts agree quite well with those expected from theory.

Table 7. Comparison of theoretical forecast RMSE's (T) with those computed from actual MVAR forecasts (C) using 1976 transformed visibility data.

	No. of	RMSE's 3-hour FCST 6-hour FCST 9-hour FCST							12-hour FC		
Station	Forecasts		7	C	T T	<u>C</u>	T C S :				
Hannover	46	0.09	0.13	0.09	0.15	0.18	0.16	0.17	?		
Bremen	46	0.09	0.14	0.14	0.16	0.15	0.16	0.12	0.17		
BoizenLurg	46	0.34	0.16	0.29	0.18	0.28	0.19	0.33	0.30		
Braunschweig	46	0.10	0.10	0.09	0.12	0.21	0.13	0.15	0.57		
Magdeburg	46	0.14	0.11	0.12	0.14	0.14	0.16	0.22	٠		
Wernigerode	46	0.25	0.18	0.19	0.20	0.19	0.20	0.26	0.1		
Weissen	46	0.12	0.13	0.16	0.15	0.19	0.16	0.22	0.17		

It was found that during the forecast periods, a much larger number of zero visibilities (resulting in a transformed variable value of one) were actually observed at Boizenburg than at any other station. In Figure 2b we can see that such observations would result in an increase in variance and thus in the RMSE's for the transformed visibilities.

The RMSE comparison for 58 temperature forecasts is displayed in Table 8 while those for 140 wind forecasts are shown in Tables 9 and 10. We can see in Tables 8 and 9 that the computed RMSE's are slightly larger than their theoretical counterparts for the temperature and u-wind MVAR forecasts. In no case, however, are these differences significant. The v-wind MVAR forecasts, whose RMSE's are shown in Table 10, are consistently

Table 8. Comparison of theoretical forecast RMSE's (T) with those computed from actual MVAR forecasts (C) using 1976 temperature data.

		RMSE 15							
Station	Forecasts	3-hour	· FCST	6-hour C	· FCST	9-hour C	- FOST	12-hou	r FCST
Hannover	58	1.65	1.50	2.25	2.08	2.94	2.39	2.79	2.71
Bremen	58	1.71	1.53	2.07	2.02	2.45	2.31	2.72	2.57
Boizenburg	58	1.61	1.62	1.98	2.08	2.31	2.36	2.25	2.57
Braunschweig	58	1.54	1.42	2.11	1.93	2.50	2.24	2.55	2.50
Magdeburg	58	1.74	1.53	2.29	2.00	2.44	2.30	2.43	2.68
Wernigerode	58	2.18	1.68	2.53	2.18	2.82	2.49	2.81	2.72
Weissen	58	1.93	1.79	2.59	2.28	2.57	2.56	2.26	_2.75

better than those expected from theory. In summary, we have seen in Tables 5 - 10 that for the most part, when tested upon 1976 observations, the forecasts produced by the six ninth order variable-at-a-time MVAR models (developed using 1972-1974 data) agree quite well with what one would expect theoretically.

Table 9. Comparison of theoretical forecast RMSE's (T) with those computed from actual MVAR forecasts (C) using 1976 u-wind data.

		<b>.</b> .	F007	RMSE's (msec ) 6-hour FCST 9-hour FCST					
Station	Forecasts	3-hour C	FCS1	6-hour	FCST	9-hour C	FUST	12-hou 	T FUST
Hannover	140	2.02	1.58	2.32	2.09	2.97	2.42	2.99	2.71
Bremen	140	2.56	1.78	2.87	2.28	3.26	2.60	3.42	2.87
Boizenburg	140	1.95	1.96	2.31	2.23	2.71	2.49	2.69	2.66
Braunschweig	g 140	1.74	1.51	2.31	1.95	2.74	2.26	3.01	2.50
Magdeburg	140	1.52	1.53	2.34	1.88	2.65	2.16	2.87	2.36
Wernigerode	140	2.17	1.91	2.71	2.27	2.81	2.53	2.95	2.72
Weissen	140	1.99	1.97	2.65	2.29	2.97	2.57	3.17	2.77

Table 10. Comparison of theoretical forecast RMSE's (T) with those computed from actual MVAR forecasts (C) using 1976 v-wind data.

	RMSE's (msec <sup>-1</sup> )								
Station	Forecasts	<u>3-hour</u>	FCST	6-hour	FCST	9-hour	FCST T	12-hou	r FCST
Hannover	140	1.32	1.41	1.41	1.74	1.78	1.97	1.80	2.13
Bremen	140	1.83	1.75	2.13	2.17	2.48	2.41	2.52	2.62
Borzenburg	140	1.29	1.73	1.45	1.96	1.59	2.12	1.68	2.26
Braunschweig	140	1.32	1.42	1.43	1.70	1.77	1.90	1.72	2.03
Magdebung	160	1.26	1.59	1.33	1.83	1.00	2.01	1.78	2.17
Wernigerode	140	1.90	1.93	1.94	2.18	2.25	2.34	2.05	2.47
Weissen	140	1.45	1.57	1.56	1.82	1.38	2.01	1.96	2.15

Finally, in the next table we will demonstrate how confidence intervals can be placed about MVAR predictions using two visibility forecasts made with the variable-at-a-time model. From the error analysis of the actual forecasts, whose results are outlined in Tables 5 - 10, we conclude that in practice the MVAR models make predictions much like we would expect from theory. Confidence intervals (C.I.) to be placed about the MVAR predictions can be computed by multiplying a constant (varying in size depending on the percent C.I. desired) by the square root of the estimated forecast-step prediction error variance. Since this is equivalent to multiplying that constant by the theoretical EMSL's snown in Tables 5 - 10, we can see that, as one would expect, larger and larger C.I.'s will be determined as the forecast-step is increased.

The results of two visibility forecasts made using the variableat-a-time MVAR model are shown in Table 11. The forecasts and confidence intervals have been transformed back into normal units (km). The 12-hour

Table 11. A comparison of MVAR visibility forecasts (F) and 80% confidence intervals (in parenthesis) with the actual observed visibilities (A).

<u>Station</u>	3-hour F A	Forecast Time - 6-hour F A	18Z, March 29, 9-hour F A	
Hannover	20+ 20+	7.8 20	7.1 8	5.3 7
	(3.9,20+)	(3.1,20+)	(3.0,20+)	(2.5,20+)
Bremen	20+ 20	20+ 20	11 20	5.7 8
	(3.7,20+)	(3.2,20+)	(3.1,20+)	(2.6,20+)
Boizenburg	7.5 18 (3.0,20+)		6.7 12 (2.6,20+)	4.5 6 (2.1,20+)
Braunschweig	20+ 20	20+ 15	9 15	8.8 9
	(4.3,20+)	(3.8,20+)	(3.5,20+)	(3.3,20+)
Magdeburg	20+ 16 (4.1,20+)	20+ 16 (3.5,20+)	6.9 12 (2.9,20+)	
Wernigerode	4 20	0.5 0	0.6 0	4.9 12
	(2.0,20+)	(0., 1.3)	(0., 1.5)	(2.1,20_)
Weissen		7.3 20 (3.0,20+)		
Station	3-hour F A	Forecast Time - 6-hour F A	- 06Z, April 16, 9-hour <u>F</u> A	1976 12-hour F A
Hannover	1.1 0.4		3 10	3.2 8
Bremen	1.3 1.5	2.2 6	2.5 8	3.1 9
	(0.7,2.1)	(1.3,4.2)	(1.4,5.2)	(1.7,20+)
Boizenburg	0.7 0	1.4 7	1.8 0	2.3 10
	(0.2,1.4)	(0.6,2.6)	(0.9,3.7)	(1.1,5.5)
Braunschweig	0.9 0.1	1.9 6	2.3 7	3.0 6
	(0.5,1.3)	(1.2,2.9)	(1.5,3.8)	(1.8,6.2)
Magdeburg	0.7 3.5	1.5 6	1.8 8	2.1 6
	(0.3,1.2)	(0.8,2.4)	(1.0,3.2)	(1.2,4.1)
Wernigerode	1.8 4.5	1.8 4	3.1 6	3.2 6
	(0.9,3.4)	(0.8,3.8)	(1.5,20+)	(1.5,20+)
Weissen	1.0 4 (0.5,1.7)	1.8 6 (1.0,3.2)	2.2 10 (1.3,4.3)	2.6 8 (1.4,6.1)

period after 18Z on March 29, 1976, was basically a time of high visibilities in this case every 80° C.I. about the MVAR forecasts included the actual visibility. It is especially notable that the model predicted very well the very low visibilities actually observed at Wernigerode 6 and 9 hours after the initial time. The 12-hour period following 06Z on April 16, 1576, was one in Which visibilities were very low after 3 hours and trace sleadily improved over the rest of the period. The very low visibilities at the 3-neum mark were well forecast and for every station the visibility were predicted to improve out to 12 hours. In this case the model dis not improve the visibilities as fast as nature and only a few of the SC C.I. include the actual observations. From this table we can see that the confidence intervals can probably be best used by an actual forecaster to specify a minimum expected visibility in high visibility situations and a making expected visibility in low visibility situations. This type of interpretation of the C.I.'s is also appropriate for the other two transformed variables (ceiling height and height of first cloud laver). The customary interpretation of the C.I.'s as a range in which we expect the variable to lie can be applied to the other three variables (temperature, u-wind, and v-wind). This range was found to be the order of +2°C and +2 m/sec for a 3-hour forecast of temperature and the wind components. respectively. For 12-hour forecasts it was found that the temperature and wind ranges were about  $+ 3^{\circ}$ C and + 3.5 m/sec, respectively.

#### 5. Conclusions

In this study multivariate autoregressive climatological models were developed to be used for short-term forecasting of six atmospheric variables (temperature, visibility, u-wind, v-wind, ceiling height, and height of the first cloud layer) over a limited area in a tactical situation. After a preliminary data analysis it was found that the cloud-height variables and visibility could best be forecast if they were first transformed so that the variance of low ceiling and visibility situations be emphasized over that of high ceiling and visibility conditions. Various forecast models were investigated, and it was found that, given the tactical constraints. the best models were ninth order variable-at-a-time MVAR models in which an observation vector consisted of the values of the variable to be predicted at the seven German stations used in this study (Hannover, Bremen, Braunschweig, Boizenburg, Magdeburg, Wernigerode, and Weissen). The prediction error variance matrix and the coefficient matrices for each of the six variable-at-a-time MVAR forecast models are tabulated in Appendix A. Using these models one can expect to make 3-hour forecasts which explain approximately 95%, 75%, 60%, 55%, 45% and 45% of the variance, respectively, for temperature, u-wind, v-wind, visibility, ceiling height, and height of the first cloud layer.

The MVAR models were developed using data collected during 1972-1974. The models were then tested independently using 1976 observations and it was found that the actual forecast errors agree quite well with what would be theoretically predicted. Using the estimated prediction error variances, confidence intervals were determined to be placed about the MVAR forecasts. It was found that 80% C.I.'s of  $\pm 2^{\circ}$ C and  $\pm 2$  m/sec could

be placed about the 3-hour forecasts of temperature and the wind components. respectively. Due to the variable transformation made upon the visibility and cloud height variables, it was found that the confidence intervals could be best used to determine minimum expected visibilities (or cloud heights) in high visibility (or ceiling) situations and to determine maximums in the peor visibility (low ceiling) situations.

#### 6. References

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## APPENDIX A

# COVARIANCE AND COEFFICIENT MATRICES FOR THE SIX VARIABLE-AT-A-TIME MVAR MODELS

VARIABL	E-AT-A-TI	HE MVAR	MODEL FOR	TEMPERATI	JRE	MODEL OR	DER IS 9
ONE-STEP	PREDICTIO	ON ERROR	COVARIANO	CE MATRIX			
2.2390 1.3424	1.3424	1.1723	1.3838 1.0036	1.0775 0.7832	1.4253 0.9985		
1,1723	1.1171	2.6270	1.0690	1.0708	1.1669	1.604	9
1.3838 1.0775	1.0037 0.7833	1.0691	2.0247 1.1673	1.1673 2.3475	1.4253		
1.4253	0.4986	1.1669	1.4253	1.3710	2.8232	1.4082	2
1.2031	1,9633	1.6049	1.2156	1.4995	1.4082	3. 190:	2
COEFFICI	ENT MATRI	<b>1.</b> A 1					
-0.5150			-0.0477	0.0406	-0.2020		
		-0.0952	-0.0068	0.0339	-0.1055		
		-0.4113 -0.0813	0.0529 -0.4863	0.0214	-0.0723 -0.1508		
-0.1544	-0.0695	-0.1085	-0.1129	-0.3041	-0.2153	-0.1029	<del>,</del>
		-0.0531 -0.2359	-0.0294 0.0111	-0.0057 -0.0222	-0.6194		
-0.1347	-0.0576	- ( • 2 3 3 9	0.0111	-0.0222	-(•00)	- (· • ) j j ;	-
COEFFICE	ENT MATRI	X A2					
0.0643			0.0165	0.0396	0.0200		4
		-0.0182	0.0366	0.0346	-0.0149		
0.1740 0.1805		-0.0832 -0.0096	-0.0680 -0.1213	0.0329 0.0488	-0.0260 0.0105		
0.1533	J. 0576	0.0342	-0.0246	-0.0134	-0.0081	0.0037	7
0.1592 0.14 <b>3</b> 7		-0.0617 0.0181		0.0395 0.0087	-0.0502 -0.0518		
0.1437	0.0004	0.0101	-0.0344	0.0067	-0.0310	0.0132	<i>(</i> .
COEFFICE	ENT MATRI	E & . Y.					
0.0240	-0.0041 -	-0.0218	-0.0147	0.0039	-C.0099	0.0176	S
0.0123	-0.0330	0.0252	0.0115	-0.0219	-0.0067	0.0394	<b>‡</b>
		0.0139 -0.0332	0.0426 -0.0401	0.0235 0.0372	0.0272		
		-0.0134	0.0949	-0.0065	-0.0220		
		-0.0132	0.0528	0.0667	0.0026		
-0.0,89	-0.0431	0.0075	0.0569	0.0228	0.0070	0.0990	)
COEFFICIENT MATRIX A4							
0.0080	-0.0069	0.0366	0.0219	0.0034	-0.0200	0.0022	2
	-0.0244	0.0068	0.0304	0.0054	-0.0136		
1.0449		-0.0871	-0.0711	0.0137	-0.0658		
J.3183 3.3145	0.0059 0.0062	0.0311	-0.0163 0.0112	-0.0134 -0.0597	-0.0496		
-0.0433		-0.0757	0.0112	-0.0397	-0.0400		
0.0352		-0.0209	-0.0149	-0.0436	-0.0429		

## COEFFICIENT MATRIX A5

-0.0925	-0.0017	0.0201	-0.0072	0.0275	-0.0197	0.0020
-0.0421	-0.0392	0.0252	-0.0013	-0.0000	-0.0097	0.0110
-0.1145	-0.0149	0.0764	0.0907	-0.0280	0.0682	-0.0268
-0.0299	-0.0002	-0.0127	-0.0614	0.0327	0.0256	0.0278
-0.0721	0.0082	0.0294	-0.0172	-0.0189	0.0523	0.0520
-0.1080	0.04.18	0.1245	0.0127	-0.0167	0.0740	0.0258
-0.0977	-0.0309	0.0313	-0.0093	0.0175	0.0322	0.0209

## COEFFICIENT MATRIX A6

-0.0133	-0.0410	0.0411	0.0027	-0.0148	-0.0054	-0.0022
0.0071	-0.0698	0.0277	-0.0232	-0.0138	0.0115	0.0248
0.0584	-0.0465	-0.0673	-0.0469	0.0130	-0.0806	0.0426
0.0205	-0.0224	0.0252	-0.0520	-0.0011	-0.0151	-0.0178
0.0234	-0.0542	-0.0115	0.0347	-0.0362	-0.0232	-0.0152
0.0844	-0.0893	-0.0623	-0.0166	-0.0241	-0.1493	0.0339
0.0143	-0.0217	0.0414	0.0484	-0.0351	-0.0279	-0.C326

## COEFFICIENT MATRIX A7

-0.0029	-0.0365	-0.0428	0.0541	-0.0222	0.0434	-0.0101
0.0598	-0.0557	-0.0800	0.0474	-0.0425	0.0608	-0.0137
-0.0289	-0.0335	-0.0113	0.0385	-0.0367	0.1244	-0.0453
0.0060	-0.0338	-0.0010	0.0289	-0.0220	0.0456	0.0024
-0.0139	-0.0409	0.0244	0.0503	-0.0450	0.0760	-0.0132
-0.0326	-0.0078	-0.0146	0.0565	-0.0087	0.0698	-0.0249
-0.0394	-0.0672	-0.0108	0.0475	-0.0163	0.1248	-0.0724

## COEFFICIENT MATRIX A8

-0.0956	-0.0360	-0.0136	-0.0697	-0.0575	-0.0245	-0.0712
-0.0491	-0.0596	-0.0064	-0.0547	-0.0622	-0.0653	-0.0334
-0.0284	-0.0664	-0.0779	0.0103	-0.0400	-0.0977	-0.0461
-0.0252	-0.0158	-0.0302	-0.1280	-0.0823	-0.0457	-0.0497
-0.0514	-0.0164	-0.0389	-0.0590	-0.1082	-0.0982	-0.0820
-0.0771	0.0069	0.0145	-0.0757	-0.1425	-0.0459	-0.0456
-0.1077	-0.0097	-0.0354	-0.0592	-0.0799	-0.0779	-C.1176

## COEFFICIENT MATRIX A9

0.0553	0.0798	0.0320	0.0306	0.0364	0.0533	0.0426
0.0869	0.0310	0.0551	0.0102	0.0079	0.0996	0.0118
0.0992	0.0506	0.0521	-0.0242	0.0146	0.0755	0.0520
0.0749	0.0557	0.0560	-0.0012	0.0537	0.0692	0.0208
0.1017	0.0225	0.0682	0.0192	0.0225	0.0973	0.0509
0.1518	0.0444	0.0368	0.0044	0.0384	0.0340	0.0589
0.1420	0.0514	0.0778	0.0082	0.0191	C.0947	0.0559

VARIABLE	E-AT-A-TIME	MVAR	MODEL FOR	U-WIND	MODEL	ORDER IS
ONE-STEP	PREDICTION	ERROR	CCVARIAN	CE MATRIX		
2.5136 1.3577 0.7471 1.1606 0.7448 0.9397 0.6056	3.1844 0. 0.8617 3 0.9717 0 0.5516 0 0.7827 0	.7470 .8616 .8494 .6695 .7303 .5848	1.1605 0.9717 0.6696 2.2772 0.8118 0.9385 0.5583	0.7448 0.5516 0.7303 0.8118 2.3347 0.8536 0.7419	0.9897 0.7826 0.5848 0.9386 0.8537 3.6600 C.5087	0.6056 0.6750 0.9971 0.5583 0.7419 0.5087 3.8797
COEFFICE	ENT MAMRIX .	A T				
-0.2407 -0.1467 -0.2544 -0.2349 -0.2357	-0.5394 -0 -0.2720 -0 -0.2311 -0 -0.1071 -0 -0.1238 -0	.0295 .0417 .2264 .0330 .0387 .0290 .1432	-0.1455 -0.0948 -0.0510 -0.3417 -0.1028 -0.0479 -0.0874	-0.0714 0.0116 -0.0798 -0.0463 -0.3061 -0.0932 -0.1719	-0.1141 -0.0299 -0.0474 -0.1305 -0.1609 -0.4301 -0.0470	-0.0327 -0.0184 -0.0961 -0.0141 -0.0543 -0.0128 -0.2457
COEFFICI	ENI MATRIX	<b>A</b> 2				
-0.0080 0.0491 0.0075 0.0512 0.0414 0.0866 0.0629	-0.0430 0 0.0120 -0 0.1064 -0 0.0627 -0 0.0273 -0	.0180 .0205 .1045 .0077 .0246 .0111	0.0174 0.0535 -3.0023 -3.1098 0.0138 0.0006 -3.0126	0.0125 0.0471 0.0619 0.0066 -0.0478 0.0458 -0.0116	0.0595 0.0314 0.0177 0.0564 0.0152 -0.0833 0.0691	0.0193 0.0047 0.0094 -0.0049 -0.0005 0.0218 -0.0518
CUEFFICI	ENT MATRIX	A 3				
0.0291 0.0269 0.0754 -0.0132 0.0661	0.0130 -0 -0.0046 0 0.0307 0 -0.0107 -0	.0091 .0251 .0481 .0231 .0182 .0140	0.0094 0.0404 0.0176 -0.0246 0.0715 0.0422 0.0324	0.0112	-0.0165 -0.0030 0.0569 -0.0066 -0.0065 -0.0608 0.0106	-0.0013 -0.0153 -0.0250 0.0118 -0.0021 0.0077 -0.0311
OFFFICI	ENT MATRIX	A 4				
-0.0157 -0.0091 -0.0254 -0.0387	-0.0432	.0293 .0154 .0490 .0221 .0145 .0464	-0.0299 0.0103 0.0135 -0.0672 -0.0039 -0.0020 -0.0046	0.0155 -0.0023 -0.0114 0.0129 -0.0218 -0.0038 -0.1643	0.0369 0.0033 -C.0088 0.0175 -0.0020 -0.0007	0.0237 0.0075 0.0135 -0.0060 -0.0032 0.0075 -0.0369

-0.0448	0.0321	-0.0225	0.0272	-0.0085	-0.0072	-0.0111
-0.0182	0.0039	0.0045	0.0199	0.0018	0.0004	-0.0039
-0.0468	0.0395	0.0144	-0.0129	0.0481	0.0196	0.0215
0.0215	0.0375	-0.0011	-0.0141	0.0321	-0.0114	0.0225
-0.0147	0.0142	0.0173	0.0547	-0.0115	-0.0199	0.0188
0.0223	-0.0162	0.0144	0.0219	-0.0109	-0.0363	0.0072
0.0039	0.0202	0.0155	0.0376	0.0638	-0.0046	-0.0167

# COEPPICIENT MATRIX A6

0.0055	-0.0258	0.0190	-0.0018	-0.0172	-0.0085	0.0046
-0.0140	-0.0432	0.0188	-0.0231	-0.0050	0.0017	0.0080
0.0589	0.0006	-0.0281	-0.0539	-0.0589	-0.0130	0.0125
0.0228	-0.0315	0.0269	-0.0719	-0.0252	-0.0009	-0.0034
0.0381	0.0182	-0.0098	-0.0497	-0.0267	0.0174	-0.0141
0.0398	0.0072	-0.0049	-0.0118	-0.0572	-C.0224	0.0030
0.0228	-0.0110	-0.0011	-0.0349	-0.0219	0.0214	-0.0224

# COEFFICIENT MATRIX A7

-0.0298	0.0086	-0.0111	-0.0251	0.0295	-0.0080	-0.C244
-0.0162	-0.0388	-0.0249	-0.0068	0.0548	-0.0171	-0.0347
-0.0489	0.0186	-0.0437	0.0261	0.0083	0.0150	-0.0074
-0.0105	0.0144	-0.0115	-0.0448	0.0281	0.0318	-0.0120
-0.0763	0.0255	-0.0211	0.0390	0.0057	-0.0071	0.0006
0.0007	-0.0319	-0.0396	0.0076	0.0229	-0.0081	-0.0119
-0.0496	0.0135	-0.0132	-C.0086	0.0305	-0.0133	-0.0208

### COEPFICIENT MATRIX A8

0.0021	0.0168	-0.0094	-0.0379	-0.0445	-0.0104	-0.0001
0.0027	-0.0021	-0.0125	-0.0579	-0.0207	0.0045	-0.0000
0.0075	0.0203	-0.0400	-0.0348	-0.0200	-0.0050	-0.0134
-0.0246	-0.0022	-0.0419	-0.0412	-0.0549	-0.0281	-0.0163
0.0001	0.0049	-0.0082	-0.0233	-0.0463	-0.0154	-0.0171
0.0020	0.0119	-0.0180	-0.0249	-0.0120	-0.0521	0.0042
-0.0064	0.0272	-0.0120	-0.0476	-0.0252	0.0106	-0.0236

# COFFFICIENT MATRIX A9

-0.0081	0.0059	-0.0103	0.0889	0.0334	0.0131	-0.0060
0.0318	-0.0134	-0.0012	0.0670	0.0375	-0.0105	-0.0036
0.0088	0.0152	0.0068	0.0729	0.0154	0.0097	0.0076
0.0161	0.0444	0.0052	0.0427	0.0366	0.0375	0.0094
-0.0015	0.0165	-0.0093	0.0781	0.0368	0.0154	0.0058
-0.0197	0.0174	-0.0024	0.0786	0.0335	-0.0125	0.0194
0.0198	0.0032	0.0103	0.0458	0.0264	0.0465	-0.0012

ONF-STEP PREDICTION ERROR COVARIANCE NATEIX	VAPIAB	LE-AT-A-TIME	MVAR MODEL	FOR V-WIND	MODEL	ORDER IS
C.8955 3.0762 0.5991 0.4587 0.4081 0.3197 0.4387 0.5895 0.5895 0.5891 2.9894 0.5059 0.4896 0.2117 0.5842 0.7087 0.4587 0.5059 2.0322 0.6705 0.5176 0.5176 0.4081 0.4996 0.6705 2.5116 0.6577 0.6002 0.5277 0.3197 0.2117 0.5178 0.6577 3.7166 0.4081 0.4981 0.4996 0.6705 0.6577 3.7166 0.4081 0.4981 0.4982 0.5673 0.6009 0.4353 2.4874 0.4520 0.4338 0.5942 0.5673 0.6009 0.4353 2.4874 0.4952 0.4338 0.5942 0.5673 0.6009 0.4353 2.4874 0.4952 0.4338 0.5942 0.5673 0.6009 0.4353 2.4874 0.4952 0.4338 0.5942 0.5673 0.6009 0.4353 0.6009 0.4353 0.00060 0.0209 0.00060 0.0209 0.00060 0.0209 0.00060 0.0209 0.00060 0.0209 0.00060 0.0209 0.00060 0.2109 0.00060 0.0209 0.00060 0.0209 0.00060 0.2109 0.00060 0.2109 0.00060 0.0209 0.00060 0.0209 0.00060 0.0209 0.00060 0.0209 0.00060 0.0009 0.00060 0.0009 0.00060 0.0	ONE-STE	P PREDICTION	ERROR COVAR	IANCE MATRIX		
0.5895						
0.5176						
0.5277	C.7087	0.4587 0.	.5059 2.03		0.5178	0.5673
CORPFICIENT HATRIX A2  -0.0366    -0.01806    -0.0345    -0.0291    -0.0345    -0.0345    -0.0291    -0.0345						
CORPRICIENT MATRIX A1  -0.3342 -0.3204 -0.0893 -0.0854 -0.0284 0.0162 -0.0345 -0.1316 -0.6586 -0.0335 -0.0896 -0.0284 0.0162 -0.0345 -0.1214 -0.2677 -0.2575 -0.0820 -0.0660 -0.0220 -0.0707 -0.2151 -0.1891 -0.0941 -0.2721 -0.0707 -0.0367 -0.0874 -0.1640 -0.1425 -0.0833 -0.1899 -0.2004 -0.0940 -0.927 -0.737 -0.1621 -0.1906 -0.1309 -0.1699 -0.2004 -0.0940 -0.						
-0.3342 -0.3204 -0.0893 -0.0854 -0.0345 -0.0291 -0.7670 -0.1306 -0.6586 -0.0335 -0.0496 -0.0284 -0.0162 -0.0345 -0.1214 -0.2677 -0.2575 -0.0820 -0.0660 -0.0229 -0.0706 -0.2151 -0.1891 -0.0941 -0.2721 -0.0707 -0.0367 -0.0876 -0.1640 -0.1425 -0.0833 -0.1899 -0.2004 -0.0880 -0.1970 -0.1506 -0.1506 -0.0778 -0.0992 -0.0671 -0.3549 -0.1234 -0.1621 -0.1806 -0.1309 -0.1272 -0.0732 -0.0435 -0.0234 -0.01621 -0.1806 -0.1309 -0.1272 -0.0732 -0.0435 -0.0234 -0.0366 -0.0160 -0.0278 -0.0284 -0.0067 -0.0059 -0.0371 -0.0833 -0.0584 -0.0877 -0.0342 -0.0100 -0.0099 -0.0244 -0.0261 -0.0579 -0.0368 -0.0791 -0.0007 -0.0009 -0.0244 -0.0261 -0.0582 -0.0104 -0.0682 -0.0152 -0.0018 -0.0284 -0.0284 -0.0274 -0.0284 -0.0224 -0.0087 -0.0284 -0.0087 -0.00				0.000	<b>2</b> • • • • • • • • • • • • • • • • • • •	£ • ·
-0.1306 -0.6586 -0.0337 -0.0496 -0.0284	COEFFIC	IENT HATPIX :	1.1			
-0.1214 -0.2677 -0.2575 -0.0829 -0.0660 -0.0227 -0.0767 -0.2151 -0.1891 -0.0941 -0.2721 -0.0707 -0.0367 -0.0876 -0.1640 -0.1425 -0.0833 -0.1899 -0.2004 -0.0880 -0.1309 -0.1973 -0.1506 -0.0778 -0.0992 -0.0671 -0.3580 -0.0230 -0.1621 -0.1806 -0.1309 -0.1272 -0.0732 -0.0435 -0.0435 -0.0316 -0.01621 -0.1806 -0.1309 -0.1272 -0.0732 -0.0435 -0.0336 -0.0356 -0.0160 0.0278 0.0284 -0.0667 -0.0059 0.0371 0.0833 0.0584 -0.0877 -0.0342 -0.0100 0.0009 0.0244 0.0833 0.0584 -0.0877 -0.0342 -0.0100 0.0009 0.0244 0.0164 0.0682 0.0152 0.0018 -0.0284 0.0214 0.0836 -0.0791 0.0007 0.0009 0.0244 0.0104 0.0682 0.0152 0.0018 -0.0284 0.0214 0.0837 -0.0228 0.0656 0.0278 0.0783 0.0275 -0.0636 -0.0128 -0.0127 -0.0096 0.0214 0.0837 0.0153 -0.0153 -0.0225 0.0086 0.0276 0.0099 0.0128 0.0225 0.0086 0.0278 0.0275 -0.0096 0.0242 0.0128 0.0336 0.0287 -0.0086 0.0331 0.0472 0.0366 -0.0127 -0.0096 0.0366 -0.0128 0.0399 0.0301 0.0472 0.0366 -0.0212 0.0224 0.0127 0.0086 0.0301 0.0472 0.0366 -0.0212 0.0224 0.0127 0.0086 0.0301 0.0472 0.0366 -0.0212 0.0224 0.0127 0.0041 0.0225 0.0198 0.0162 -0.0085 -0.0040 0.0280 -0.0085 0.0336 0.0287 -0.0085 0.0336 0.0287 -0.0086 0.0301 0.0472 0.0366 -0.0212 0.0224 0.0127 0.0041 0.0225 0.0198 0.0162 -0.0085 -0.0040 0.0280 -0.0077 0.0184 0.0242 0.0256 -0.0039 -0.0132 0.0096 0.0177 0.0184 0.0242 0.0256 -0.0039 -0.0132 0.0096 0.0177 0.0184 0.0242 0.0256 -0.0039 -0.0132 0.0096 0.0174 -0.0085	-0.3342	-0.3204 -0.	.0893 -0.08	54 -0.0345	-0.0291	
-0.2151 -0.1891 -0.0941 -0.2721 -0.0707 -0.0367 -0.0836 -0.1640 -0.1425 -0.0833 -0.1899 -0.2004 -0.0990 -0.1373 -0.1506 -0.0778 -0.0992 -0.0671 -0.3548 -0.0990 -0.1621 -0.1806 -0.1309 -0.1272 -0.0732 -0.0435 -0.0730 -0.1621 -0.1806 -0.1309 -0.1272 -0.0732 -0.0435 -0.0730 -0.0956 -0.0035 -0.0435 -0.0732 -0.0435 -0.0730 -0.0956 -0.0035 -0.0956 -0.0035 -0.0284 -0.0367 -0.0059 -0.0371 -0.0833 -0.0584 -0.0877 -0.0342 -0.0100 -0.0099 -0.0371 -0.0833 -0.0579 -0.0384 -0.09791 -0.0007 -0.0009 -0.0244 -0.0104 -0.0682 -0.0152 -0.0018 -0.0284 -0.0214 -0.0887 -0.0284 -0.0967 -0.0009 -0.0036 -0.0244 -0.0284 -0.0152 -0.0104 -0.0682 -0.0152 -0.018 -0.0284 -0.0214 -0.0887 -0.0128 -0.0284 -0.0153 -0.0127 -0.0099 -0.0128 -0.0428 -0.0104 -0.0682 -0.0153 -0.0127 -0.0096 -0.0214 -0.0887 -0.0127 -0.0096 -0.0124 -0.0087 -0.0127 -0.0096 -0.0127 -0.0096 -0.0128 -0.0127 -0.0096 -0.0128 -0.0127 -0.0096 -0.0128 -0.0127 -0.0096 -0.0128 -0.0127 -0.0096 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0128 -0.0099 -0.0132 -0.0099 -0.0132 -0.0099 -0.0134 -0.0085 -0.0034 -0.0036 -0.0038 -0.0036 -0.0033 -0.0138 -0.0036 -0.0038 -0.0038 -0.0038 -0.0033 -0.0138 -0.0035 -0.0039 -0.0134 -0.0134 -0.0134 -0.0155						
-0.1640 -0.1425 -0.0833 -0.1899 -0.2004 -0.0980 -0.133 -0.1973 -0.1506 -0.0778 -0.0992 -0.0671 -0.3548 -0.0348 -0.03548 -0.03548 -0.03548 -0.0733 -0.1621 -0.1806 -0.1309 -0.1272 -0.0732 -0.0435 -0.0733 -0.0435 -0.0733 -0.0435 -0.0733 -0.0435 -0.0733 -0.0435 -0.0733 -0.0435 -0.0733 -0.0435 -0.0733 -0.0435 -0.0733 -0.0356 -0.0160 0.0278 0.0284 -0.0067 -0.0059 0.0371 0.0833 0.0584 -0.0877 -0.0342 -0.0100 0.0009 0.0344 0.0284 -0.0579 0.0308 -0.0791 0.0007 0.0009 0.0366 -0.0104 0.0682 0.0152 0.0018 -0.0284 0.0214 0.0686 -0.0164 0.0682 0.0152 0.0018 -0.0284 0.0214 0.0686 -0.0153 -0.0783 0.0275 -0.0638 -0.0121 0.0074 0.0284 0.0153 -0.0096 0.0216 -0.0428 0.0336 0.0277 -0.0638 -0.0123 0.0099 -0.0123 0.0099 0.0357 0.0153 -0.0127 -0.0096 0.0216 -0.0428 0.0301 0.0472 0.0306 -0.0170 0.0293 0.0099 -0.0128 0.0999 0.0005 0.0336 0.0287 -0.0080 0.0301 0.0472 0.0306 -0.0212 0.0224 0.0127 0.0084 0.0225 0.0198 0.0162 -0.0085 -0.0404 0.0280 -0.0085 -0.0042 0.0225 0.0198 0.0162 -0.0085 -0.0404 0.0280 -0.0042 0.0242 0.0256 -0.0039 -0.0132 0.0096 0.0177 0.0184 0.0242 0.0256 -0.0039 -0.0132 0.0096 0.0174 -0.0085 0.0036 0.0036 0.0033 0.0138 0.0242 0.0242 0.0256 -0.0039 -0.0132 0.0096 0.0174 -0.0085 0.0036 0.0033 0.0138 0.0035 0.0036 0.0033 0.0138 0.0035 0.0036 0.0033 0.0138 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0035 0.0036 0.0036 0.0036 0.0035 0.0036 0.0035 0.0036 0						
-0.1621 -0.1806 -0.1309 -7.1272 -0.0732 -0.0435 -0.0777  COEFFICIENT MATRIX A2  -0.0056	-0.1640	-0.1425 -0.	.0833 -0.18	99 -0.2004	-0.0887	
COEFFICIENT MATRIX A2  -C.0056						
-C.0056	-3.1021	<b>~U.</b> 1606 - U.	. 1309 - 7. 12	12 -0.0132	+0.0435	•
C.0356 -0.0160	COEFFIC	IENT MATRIX A	A 2			
0.0833	-0.0056	0.0325 0.	.0315 -0.03	40 0.0065	-0.0007	0.0052
0.0261 0.0579 0.0308 -0.0791 0.0007 0.0009 0.0036   0.0104 0.0682 0.0152 0.0018 -0.0284 0.0214 0.0087   -0.0228 0.0656 0.0278 0.0783 0.0275 -0.0638 -0.0721   0.0409 0.0357 0.01530127 -0.0096 0.0216 -0.0428    COEFFICIENT MATRIX A3  -0.0017 0.0574 0.0284 -0.0081 0.0183 -0.0007 -0.0160   -0.0064 -0.0177 0.0256 0.0170 0.0293 0.0099 -0.0128   0.0399 0.0302 -0.0459 0.0005 0.0336 0.0287 -0.0080   0.0301 0.0472 0.0306 -0.0212 0.0224 0.0127 0.0041   0.0225 0.0198 0.0162 -0.0085 -0.0404 0.0280 -0.0042   -0.0034 0.0453 0.0034 0.0218 -0.0167 -0.0177 0.0184   0.0242 0.0256 -0.0039 -0.0132 0.0096 0.0174 -0.0085    COEFFICIENT MATRIX A4  -0.0236 0.0071 0.0011 -0.0063 -0.0128 -0.0152 0.0044   -0.0236 0.0071 0.0011 -0.0063 -0.0128 -0.0152 0.0044   -0.0236 0.0071 0.0011 -0.0063 -0.0128 -0.0152 0.0044   -0.0106 -0.0060 0.0270 0.0038 -0.0036 0.0033 0.0138   0.0025 0.0100 -0.0420 -0.0109 -0.0117 0.0134 0.0155						
C.0104						
COEFFICIENT MATRIX A3  -0.0017	0.0104					
COEFFICIENT MATRIX A3  -0.0017						
-0.0017	0.0409	0.9357 V	.0153 ~ .01	27 -0.0096	0.021h	-U+1,427
-C.0064 -C.0177 0.0256 0.0170 0.0293 0.0099 -G.0128 0.0099 0.0302 -0.0459 0.0005 0.0336 0.0287 -0.0080 0.0301 0.0472 0.0306 -0.0212 0.0224 0.0127 0.0041 0.0225 0.0198 0.0162 -0.0085 -0.0404 0.0280 -0.0042 -0.0034 0.0453 0.0034 0.0218 -0.0167 -0.0177 0.0184 0.0242 0.0256 -0.0039 -0.0132 0.0096 0.0174 -0.0085 -0.0036 0.0031 0.0085 -0.0036 0.0033 0.0138 0.0025 0.0100 -0.0420 -0.0109 -0.0117 0.0134 0.0155	COEFFIC	IENT MATRIX A	13			
0.0399 0.0392 -0.0459 0.0005 0.0336 0.0287 -0.0080 0.0301 0.0472 0.0306 -0.0212 0.0224 0.0127 0.0041 0.0225 0.0198 0.0162 -0.0085 -0.0404 0.0280 -0.0042 -0.0034 0.0453 0.0034 0.0218 -0.0167 -0.0177 0.0184 0.0242 0.0256 -0.0039 -0.0132 0.0096 0.0174 -0.0085 -0.0036 0.0031 0.0038 -0.0132 0.0096 0.0174 -0.0085 -0.0166 -0.0060 0.0270 0.0038 -0.0036 0.0033 0.0138 0.0025 0.0100 -0.0420 -0.0109 -0.0117 0.0134 0.0155						
0.0301 0.0472 0.0306 -0.0212 0.0224 0.0127 0.0041						
C.0225						
0.0242 0.0256 -0.0039 -0.0132 0.0096 C.0174 -0.0085  COEPPICIENT MATRIX A4  -0.0236 0.0071 0.0011 -0.0063 -0.0128 -C.0152 0.0044 -0.0106 -0.0060 0.0270 0.0038 -0.0036 0.0033 0.0138 0.0025 0.0100 -0.0420 -0.0109 -0.0117 0.0134 0.0155					0.0280	-0.0042
COEPPICIENT MATRIX A4  -0.0236						-0.0184
-0.0236				32 3433		3 <b>4</b> (1 <b>6</b> 17 5
-0.0106 -0.0060 0.0270 0.0038 -0.0036 0.0033 0.0138 0.0925 0.0100 -0.0420 -0.0109 -0.0117 0.0134 0.0155	COEPFIC	IENT MATRIX A	14			
0.0025  0.0100  -0.0420  -0.0109  -0.0117  0.0134  0.0155						
-0.0129		0.0040 -0.	0203 -0.03	-0.0170		
0.0101 -0.0116 0.0174 -0.0158 -0.0042 0.0010 -0.0003	0.0101	-0.0116 0.	.0174 -0.01	58 -0.0042	0.0010	-0.0003
-0.0053 -0.0448 0.0275 0.0373 -0.0094 -0.0129 0.0016 0.0114 0.0020 -0.0011 -0.0099 -0.0115 -0.0026 -0.0056						

-0.0069 0.0104 -0.0121 0.0043 -0.0127 -0.0280 0.0000	0.0035	-0.0186 -0.0020 0.0016 0.0030 -0.0089 -0.0157 0.0123	0.0115 0.0125 0.0090 0.0327 -0.0064 0.0343 0.0023	0.0020 0.0086 0.0331 0.0286 0.0130 0.0068 0.0248	0.0239 0.0101 0.0097 -0.0238 -0.0163 -0.0290 -0.0068
COEFFIC	IENT MATRIX A6				
-0.0037 -0.0167 0.0016 0.0052 0.0076 -0.0137 0.0098	-0.0127	-0.0232 -0.0265 -0.0048 -0.0345 -0.0128 -0.0069 -0.0255	0.0106 0.0224 0.0172 0.0019 0.0013 0.0189 0.0085	-0.0079 0.0130 -0.0049 0.0097 -0.0070 -0.0132 -0.0005	0.0159 0.0067 0.0214 -0.0002 0.0353 0.0490 0.0129
COEFFIC	LIENT MATRIX A7				
-0.0290 -0.0026 -0.0196 -0.0245 -0.0181 -0.0016 -0.0175	-0.0063 -0.0177 -0.0264 -0.0151 -0.0179 -0.0245 0.0056 -0.0144 0.0070 -0.0062 -0.0036 -0.0085 -0.0083 -0.0075	-0.0297 -0.0181 -0.0606	0.0056 0.0114 -0.0033 0.0023 -0.0282 0.0279 -0.0080	0.0090 0.0030 -0.0157 -0.0079 -0.0104 -0.0553 -0.0090	-0.0148 -0.0080 -0.0085 0.0002 -0.0052 -0.0498 -0.0117
COEPFIC	CIENT MATRIX A8				
-0.0033 -0.0050 0.0428 -0.0046 -0.0050 0.0681 0.0155	0.0189 -0.0198 -0.0459 0.0117 0.0085 -0.0308 0.0146 -0.0358 0.0167 -0.0262 0.0169 -0.0238 0.0087 -0.0180	-0.0132 -0.0358 -0.0409 -0.0015 -0.0095	-0.0166 -0.0241 -0.0390 -0.0354 -0.0292 0.0130 -0.0276	-0,0085 0.0067 0.0027 -0.0164 0.0007 -0.0763 -0.0139	0.0097 0.0039 -0.0067 -0.0018 -0.0032 0.0063 -0.0061
COEFFIC	CIENT MATRIX A9				
0.0251 0.0359 0.0644 0.0357 0.0250 0.0162 0.0367	0.0302 0.0096 0.0198 0.0058 0.0422 -0.0255 0.0472 0.0195 0.0454 -0.0018 0.0448 0.0169 0.0289 0.0098	-0.0255 -0.0274 0.0033 0.0156 -0.0074 0.0025 0.0131	0.0128 0.0127 0.0041 0.0039 0.0108 -0.0187 0.0121	-0.0001 -0.0091 -0.0008 -0.0078 -0.0055 -0.0113 0.0034	0.0178 0.0255 0.0191 0.0146 0.0110 0.0225 -0.0084

#### CME-STEP PREDICTION ERROR COVARIANCE MATRIX 0.0030 010157 0.0033 0.0052 0.0027 0.0016 0.0050 0.0024 0.0050 0.0187 0.0035 0.0023 0.0016 0.0011 0.0065 0.0033 0.0035 0.0241 0.0024 0.0040 0.0012 0.0019 0.0024 0.0052 0.0030 0.0018 0.0023 0.0097 0.0074 0.0018 0.9027 0.0016 0.0040 0.0030 0.0132 p.,,,,,, 0.0018 0.0335 0.0016 0.0011 0.0012 0.0018 9, 4 . 7 . ( , ^ 7 7 7 0.0034 0.0003 0.0019 0.0024 0.0065 COPPEIGNENT MATERN AT -0.046 -0.0430 -0.0339 .0.1795 -0.0362 -0.1164 -0.4523 -0.0303 ~ 7.3523 -0.0293 0.0199 -0.0325-0.0183 -0.1795-0.1359 -0.4259 -0.1396 -0.0256 -0.0959 -0.0051 -0.0864 -0.0316 -0.0901 -0.0366 -0.1018 -0.0162 -0.3845 -0.2151-0.10A4 -0.0244 -0.5623 -0.1393-0.0449 -0.0438-0.0984 0.0182 -0.4005 -0.1071 -0.04760.0182 0.0101 -0.1014-9.5600 0.0034 -0.0497 -0.0900 -0.1223 -0.0033 -0.0854 COEFFICIENT MATRIX A2 -0.0028 0.0327 0.0288 0.0392 -0.0098 0.0312 0.0495 0.0138 0.0223 3.0106 0.0236 0.0197 -0.0234 -0.0041 0.0302 -0.0107 0.0422 9.1067 0.0111 0.0034 -0.0092 0.0182 0.0263 0.0087 -0.0043 0.0321 0.0600 0.0097 0.0501 0.0581 0.0546 0.0238 -0.0627 -0.0147 0.0227 0.0223 -1.0503 0.0253 -0.0080 -0.0202 -0.0178 -0.00220.0423 0.0250 0.0029 -0.0063 0.0335 0.0271 CUEPFICIENT MATRIX A3 -0.0057 -0.0026 0.0194 0.0130 0.0078 -0.0060 -0.0135 0.0264 -0.0041 0,0101 ~ 2.0096 -0.0205 0.0122 0.0053 0.0121 0.0341 0.0001 -J.0280 0.0101 -0.0591 0.0262 -0.0083 0.0099 0.0084 -0.0116 0.0021 0.0004 -0.0300 0.0133 0.0214 -0.0071 0.0129 -0.0210 0.0083 0.0094 0.0570 0.0025 0.0238 0.0120 0.0119 -0.0454 0.0368 -0.0027 0.0192 0.0294 -0.0003 -0.0027 -0.0288 0.0122 COPPUICTENT MATRIX A4 -0.0051 0.0027 0.0076 0.0169 0.0051 -0.01890.0137 -0.0028 -0.2173 -0.0113-0.0263 0.0220 0.0037 0.0152 0.0080 -0.0323 -0.0010 -0.0043 0.0117 -0.0054 -0.0321

0.0194

0.0337

-0.0380

-0.0064

-0.0097

-0.0724

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-0.0121

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0.0078

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-0.0265

-0.0316

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0.0252

1.026B

0.0024

-0.0068

-0.0208

0.0044

-0.0051

-0.0114

0.0012

-0.0092

-0.0337	-0.0031	-0.0277	0.0130	-0.0033	0.0076	0.0060
0.0053	-0.0279	-0.0213	-0.0086	0.0277	0.0055	0.0235
0.0012	0.0118	-0.0432	0.0108	0.0558	0.0066	0.0045
-0.0351	-0.0203	0.0109	0.0189	-0.0266	0.0063	0.0082
-0.0022	-0.0056	-0.0013	0.0173	0.0230	-0.0032	0.1989
-0.0190	-0.0048	0.0099	0.0221	-0.0148	0.0681	-0.0011
0.0090	-0.0130	0.0071	-0.0043	0.0091	0.0098	-n.0202

# COEFFICIENT MATRIX A6

-0.0117	-0.0273	0.0225	0.0068	-0.0016	0.0089	0.0006
0.0290	-0.0482	0.0105	-0.0235	-0.0037	0.0140	0.0047
0.0286	-0.0182	-0.0066	-0.0061	-0.0426	0.0719	-0.0058
0.0181	-0.0036	-0.0180	-0.0442	0.0306	0.0045	0.0123
0.0100	0.0012	0.0190	-0.0358	-0.0473	-0.0020	-0.0003
-0.0149	0.0065	-0.9286	0.0014	-0.0022	0.0073	-0.0168
0.0011	0.0000	0.0070	0.0295	-0.0241	0.0016	0.0076

### COEFFICIENT MATRIX A7

-0.0218	-0.0231	-0.0113	-0.0650	-0.0305	-0.0116	-0.0240
-0.0198	-0.0080	0.0058	0.0036	-0.0407	-0.0102	-0.0031
-0.0153	-0.0199	-0.0544	-0.0113	-0.0084	-0.0122	0.0023
0.0171	-0.0176	0.0094	-0.0130	-0.0300	-0.9154	-0.0104
-0.0002	-0.0206	-0.0127	-0.0025	0.0265	-0.0052	6.0109
0.0366	-0.0426	-0.0256	0.0283	0.0289	-0.1139	-0.0325
-0.0337	-0.0458	-0.0287	0.0057	-0.0175	-0.0081	-0.0307

# COEFFICIENT MATRIX A8

-0.0584	-0.0131	-0.0045	-0.0369	-0.0499	0.0047	-0.0477
-0.0444	-0.0376	-0.0311	-0.0279	-0.0441	0.0145	-0.0579
-0.0507	-0.0395	-0.0262	0.0249	-0.0505	0.0083	-0.0296
-0.0389	-0.0168	-0.0310	-0.0312	-0.0621	0.0175	-0.0570
-0.0242	-0.0227	-0.0038	-0.0559	-0.1144	-0.0008	-0.0818
0.0009	-0.0097	0.0242	0.0270	-0.0067	-0.6131	0.0001
-0.0151	-0.0574	-0.0000	-0.0263	-0.0755	0.0029	-0.0942

# COEFFICIENT MATRIX A9

0.0212	0.0478	0.0338	0.0337	0.0678	0.0052	0.0304
0.0401	0.0287	0.0357	0.0184	0.0578	-0.0030	0.0102
0.0335	0.0287	0.0453	0.0284	0.0258	-0.0143	0.0250
0.0207	0.0422	0.0304	0.0252	0.0459	0.0120	0.0334
0.0034	0.0438	0.0259	0.0789	0.0535	0.0211	0.0407
0.0292	0.0375	0.0067	0.0244	0.0894	0.2071	-0.0277
C.0490	0.0420	0.0373	0.0160	0.0640	-0.0203	0.0549

# PERSTER PREDICTION EFFOR COVARIANCE MATRIX

0.0419	0.0122	0.0056	0.0129	0.0046	0.3074	4.20%3
0.0122	0.0440	0.0069	0.0061	0.0032	0.0025	0.0038
J.0056	0.0069	0.0298	0.0037	0.0049	0.0341	0.0081
v.0129	0.0061	0.0037	0.0293	0.0054	0.3349	1.0046
3.3046	0.0032	0.0049	0.0054	0,0282	0.006c	1.50%F
0.0054	0.0025	0.0640	6.0049	0.0068	0.0263	7. 7736
2.0051	0.0039	0.0081	0.0046	0.0658	0.0035	0,0307

#### TA XISTRAM TRAINTERFIG

-0.3669	-0.5842	+ n. n. an	4 h 144 an	-0.0319	20 0000	2.623
	ก ใจ้กิดธิ์					0.040
	-0.136C					
	-0.1123			-0.6449		
-0.0983	-0.0400	-0.0549	-0.1023	-0.3246	-1.1520	· . · · · .
-0.0818	-0.0179	-0.0252	-0.0978	-0.0126	-0.4092	~ ^ , 0 / 1 }
-2.1028	-0.9754	-0.0882	-1,0555	-0.1020	-0.0436	-" - "4

# COPPRICIENT MATRIX A2

0.0040	-0,019 <b>0</b>	-0.0373	0.0226	-0.0225	0.0657	1.0026
J.0189	•0.0553	-0.0384	0.0381	0.3074	0.0049	1,0109
7-0373	-0.0198	~0.0919	3.0274	-0.0405	0.0047	្តិព្រះ្
J.0270	-0.0301	0.0095	-0.0049	0.0075	0.0254	0.0005
J.03 <b>7</b> 8	0.0067	-0.0553	0.0026	-0.0279	-0.0055	0.0338
0.0205	-0.0013	-0.0082	0,0091	0.0203	-0.1363	0,0007
3.0319	0.0176	-0.0663	0,0036	0.0297	0.0399	-0.0228

### OBFFICIENT KATRIX A3

0.0102	0.0097	-0.0080	0.0106	0.0057	-0.0021	0.0286
7.0147	5.0124	-0.0201	0.0044	-0.0036	0.0299	-c.0109
0.0446	0.0211	0.0028	0.0130	-0.0351	0.0413	-0.0018
0.0012	9.0049	0.0207	-0.0089	-0.0123	0.0204	-0.0107
0.0280	0.0167	0.0468	-0.0072	-0.0163	-0.0047	0.0324
1.0058	-0.0042	-0.0436	-0.0016	-0.0097	-0.0041	0.0574
0.065	0.0115	0.0140	0.0146	-0.0234	0.0156	-0.0327

# OFFEICIERT MATRIX A4

7.0059	-0.0026	0.0260	-0.0174	-0.0208	0.0025	-0.0164
-0.0021	-0.0258	-0.0109	-0.0316	-0.0211	0.0132	0.0291
0139	-0.0148	-0.0535	0.0129	-0.0156	-0.0155	0.0081
. 0298	0 0030	-0.0015	0.0178	-0.0187	-0.0251	-0.0173
7.0083	-0.0072	-0.0304	0.0067	-0.0520	-0.0470	0.0030
7.0050	-0.0035	0.0180	0.0145	-0.0289	-0.0633	-0.0521
9.0034	-0.0007	-0.0677	0.0420	0.0068	-0.0626	-0.0012

-0.0258	-0.0080	0.0243	0.0177	-0.0141	-0.0044	-0.0064
-0.0126	-0.0045	0.0573	0.0180	-0.0220	-0.0085	-0.0074
-0.0137	0.0251	0.0280	-0.0072	0.0035	0.0355	0.0028
-0.0357	0.0206	0.0396	0.0130	-0.0050	0.0103	-0.0011
-0.0459	0.0111	0.0492	0.0384	0.0031	0.0138	0.0174
0.0205	0.0049	0.0358	-0.0074	-0.0466	0.0373	0.0690
-3.0324	-0.0158	0.0125	0.0125	-0.0039	0.0409	0.0033

# COEFFICIENT MATRIX A6

-0.0409	0.0127	0.0017	-0.0068	0.00 <b>77</b>	0.0123	-0.0184
0.0030	-0.0129	-0.0476	-0.0063	0.0150	0.0391	-0.0077
0.0039	-0.0269	-0.0142	0.0024	0.0288	0.0100	0.0001
-0.0099	-0.0225	0.0379	0.0147	-0.0094	-0.0047	-0.0067
0.0136	-0.0008	-0.0142	0.0083	-0.0084	-0.0026	-0.0175
-0.0106	0.0163	-0.0258	0.0084	0.0209	0.0064	-0.0186
0.0090	0.0067	0.0179	-0.0467	0.0006	0.0108	-0.0056

### COEFFICIENT MATRIX A7

0.0020	-0.0326	0.0421	-0.0247	0.0056	-0.0042	-0.0241
0.0178	-0.0102	0.0666	-0.0254	-0.0208	-0.0093	-0.0449
-C.0077	0.0076	-0.0066	0.0142	-0.0167	-0.0272	-0.0271
-0.0174	-0.0298	0.0091	-0.0282	0.0092	0.0398	-0.0042
-0.0201	-0.0255	0.0191	0.0180	-0.0118	0.0257	0.0056
0.0001	-0.0313	-0.0179	-0.0033	-0.0051	-0.0243	-0.0134
0.0038	-0.0042	0.0111	0.0210	-0.0238	0.0001	-0.0382

# COEFFICIENT MATRIX A8

-0.0108	-0.0034	-0.0158	-0.0328	-0.0495	0.0047	-0.0077
-0.0317	-0.0179	-0.0119	-0.0009	-0.0267	-0.0204	0.0092
0.0206	-0.0042	-0.0299	-0.0239	-0.0192	0.0135	-0.0072
-0.0102	0.0174	-0.0062	-0.0476	-0.0580	0.0152	-0.0335
0.0041	0.0093	-0.0100	-0.0173	-0.0202	-0.0168	-0.0050
-0.0103	0.0031	-0.0097	0.0097	-0.0189	-0.0231	-0.0072
-0.C038	0.0118	0.0025	-0.0168	-0.0096	0.0017	-0.0467

### COEPPICIENT MATRIX A9

0.0223	0.0107	0.0203	0.0129	0.0198	-0.0017	0.0307
0.0014	0.0044	0.0180	0.0049	-0.0149	0.0238	0.0303
0.0027	-0.0012	0.0073	-0.0008	0.0259	-0.0118	0.0038
0.0310	0.0085	0.0433	0.0056	0.0125	0.0076	0.0076
0.0044	0.0091	-0.0164	0.0101	-0.0030	0.0063	0.0089
-0.0006	0.0232	0.0161	0.0095	0.0329	-0.0301	0.0104
-0.0056	-0.0096	0.0093	0.0188	0.0395	-0.0137	-0.0043

# ME-STEP FRIDICTION TEROS CONTRIANCE MASSIX

2.6359	1.5	1.1034	2.00	C.1059		7 × 1 1 1
0.0132	0.0369	1.00%	1. 11.65	0.00.0		1.00.7
0030	0.0043	(,0187	0.0023	U.0025	0.0020	0.0041
0.0126	0.0065	0.0023	0.0061	0.0043	0.0041	2.72.75
	3.0020	2,0026	0.1.43	0.0244	7 . 10 <b>4 7</b>	
0.0042	0, 0011	0.0020	J. 7		6. 22.34	2.21
(623	1.1655	1.004	( . 1 . 7 9	( ) ( )		

# CONTRACTOR FOR SUPERIOR OF

4267	<b>-</b> 20		e e	~ *		
.0.1700	→ 00 - 5 / 3 / 3	14 to 1 to 2 to 2.	5.2	2. C11		
-0.0312	କ୍ଟୁ-ପ୍ରସ୍ଥ	-0.3400				
-0.2619	0.00	-0,0861	- 1 j j j	<b>-</b> ? , / ` : : : \$		
-0.0733	-0.0293	-0.0703	17	<b>-0.</b> 1210	· , , ;	-
-0.0863	0.0056	-0.0759	-0.04	<b>-0.01</b> /2	-0.3700	-0,000 m
-0.08 <b>7</b> 9	-0,0491	-0, 1747		<b>-</b> 1	the second	<u> </u>

# COPPRICIONS ARTRIV AD

2.02.12	-0.0205	6.0055	5 t		y a more	ودر ده نماند ده
0.0300	-9.9255	- 0, 3160	1.3111			
3.9391	· 9 9839	-0.0015.5	134	-0.0100	0.2000	-7.769
0.0265	-0.3056	~0,0 P.	- 1 G	<b>-0.</b> 0048	5. 150	-0.5053
		-9. 332b				1. 112.44
9,0169	-0.0148	0.0309	t: ^	0.000	-0.00	0.1038
3,0352	7.7 0303	<b>-</b> 0,10,175.	07	0.0231	40 July 2	-0.0352

# COSPETCIENT \*\*TRIX A3

0.0.97	0.0083	-0.0044	0,0213	-0.0025	0.0303	0.0241
0.0182	4.0013	-0.0260	0.1124	0.0304	0.0032	-0.0113
0.0203	1、660年後	-0.0016	-0,0109	-0.0120	0.0216	0.0168
0.0055	1.0798	-0.0090	-0.5154	0.0079	0.0176	0.0047
0.0203	0.0206	0.0435	-0.0064	-0.0018	-0.0032	0.0425
1.0108	0.0090	-0.0203	-3.0130	-0.0025	-0.0264	0.0356
5 00044	0.0274	-0.0091	0.1076	-0.0192	0.0274	-0.0353

# TORRETOTENT MATRIX A4

0.0394	0.0110	-0.0057	0.0022	-0.0320	0.0015	0.0090
0.0041	0.0040	0.0013	-0.0211	-0.0268	0.0283	0.0338
0.0335	-0.0048	-0.0508	0.0132	-0.0158	0.0160	-0.0182
0.0216	0.0014	-0.0014	0.0148	-0.0342	-0.0215	0.0090
0.0:30	-0.0081	-0.0130	-0.0332	-0.0403	-0.0324	0.0037
0.0169	-0.0347	0.0293	-0.0157	0.0030	-0.0012	-0.0298
-0.0332	-0.0075	-0.0807	0.0495	0.0140	-0.0383	-0.0080

-0.0102	-0.0198	0.0541	0.0081	-0.0216	0.0146	-0.0086	
-0.0012	-0.0223	0.0189	0.0209	-0.0395	-0.0093	-0.0068	
0.0302	0.0012	0.0351	-0.0275	-0.0175	0.0386	0.0074	
-0.0093	-0.0020	0.0459	0.0180	-0.0090	0.0094	-0.0111	
-0.0200	-0.0002	0.0282	0.0263	-0.0171	0.0131	0.0035	
0.0223	0.0112	0.0356	-0.0451	-0.0540	0.0019	0.0564	
-0.0058	-0.0026	0.0608	-0.0198	-0.0201	0.0009	0.0070	
COPPRICIONA MATRIX AC							

### COEFFICIENT MATRIX A6

-0.0078	-0.0202	0.0131	-0.0088	0.0106	0.0134	-0.0255
0.0422	-0.0241	-0.0163	-0.0453	0.0242	0.0336	0.0126
-0.0139	-0.0126	-0.0146	0.0115	0.0010	-0.0112	-0.0644
-0.0041	-0.0253	0.0230	-0.0046	0.0116	-0.0016	-0.0112
-0.0090	-0.0093	0.0140	0.0381	-0.0171	-0.0098	-0.0230
-0.0108	0.0039	-0.0089	0.0209	0.0221	0.0183	-0.0330
0.0068	-0.0110	0.0152	0.0131	0.0051	0.0268	-0.0197

### COEPFICIENT MATRIX A7

-0.0102	0.0080	0.0017	0.0015	0.0079	0.0046	-0.0257
0.0061	-0.0070	0.0233	-0.0032	-0.0163	0.0026	-0.6440
-0.0159	0.0047	-0.0115	0.0073	-0.0009	-0.0155	-0.0099
0.0001	-0.0076	0.0234	-0.0291	-0.0191	0.0392	-0.0025
-0.0159	-0.0001	0.0258	-0.0070	0.0092	0.0205	0.0219
-0.0099	-0.0085	0.0005	-0.0094	0.0016	-0.0398	0.0144
-0.0179	-0.0041	0.0082	-0.0250	-0.0023	0.0071	0.0029

### COEFFICIENT MATRIX A8

-0.0385	-0.0406	0.0325	-0.0443	-0.0326	-0.0113	-0.0187
-0.0352	-0.0563	0.0052	-0.0354	-0.0022	-0.0284	0.0094
0.0233	0.0032	-0.0255	-0.0208	-0.0088	-0.0351	-0.0090
-0.0230	-0.0087	0.0009	-0.0382	-0.0332	0.0036	-0.0443
0.0123	-0.0088	-0.0022	-0.0015	-0.0134	-0.0240	-0.0092
-0.0240	0.0090	-0.0066	0.0121	0.0012	-0.0307	C.0107
0.0015	-0.0104	0.0316	-0.0524	-0.0154	0.0251	-0.0407

# COEFFICIENT MATRIX A9

0.0324	0.0342	-0.0214	0.0381	-0.0010	-0.0090	0.0240
0.0149	0.0318	0.0003	0.0285	-0.0204	0.0126	0.0125
-0.0125	0.0038	0.0088	0.0194	0.0046	0.0366	0.0027
0.0226	0.0088	0.0297	0.0280	0.0118	-0.0046	0.0151
-0.0144	0.0276	-0.0103	0.0033	-0.0231	0.0097	-0.0032
0.0011	0.0291	-0.0030	0.0183	0.0166	-0.0314	-0.0127
-0.0106	0.0162	-0.0089	0.0411	0.0356	-0.0249	0.0061

#### AppENDIX D

# A REPORT OF THE PROPERTY OF ANALYSIS PROCEDURED

```
THIS PROGRAM IS USED TO SELECT THE PROPER ORDER MYAR MODEL AND
   DETERMINES THE COVARIANCE AND COEFFICIENT MATRICES FOR THAT MODEL
  GIVEN II NP-DIMENSIONAL OBSERVATION VECTORS. THE MAXIMUM ORDER
   MODEL CONSIDERED IS LGOLD-1. AFTER THE FINAL MVAR MODEL HAS
   SHEN DETERMINED. THE PREDICTION ERROR MATRICES FOR VARIOUS-STEP
   FURECASTS ARE COMPUTED BY SUBROUTINE ERRYAR.
      DIMENSION GAM (7,7,10), & (7,7,10), AB (7,7,10), B (7,7,10),
      BR(7, 7, 10), V(7, 8768), XMN(7), S(7,7), S3(7,7), EE(7,7), DD(7,7
       - 2 (7,7) -31 (10) , AA (7,7) , ITOM (7,7)
      NP=7
   NP IS THE NUMBER OF PREDICTOR VIRIABLES.
      4(:
   NO IS THE NUMBER OF VARIABUES TO BE PREDICTED, NO IS LESS THE
   EJUAL TO NP.
      LGOLD=10
   LGOLD IS ONE MORE THAN THE MANIMUM ORDER MVAR MODEL TO BE COMBILED
      LG=LGOLD
      II = 8768
  II IS THE NUMBER OF OBSERVATION VECTORS TO WHICH MWAR MODELS ASS
 TO BE FITTED.
      BEFORE SUBROUTINE RHJONS IS CALLED FOR THE FIRST TIME THE
  OBSERVATION VECTORS ARE PLACED IN ARRAY X DIMENSIONED NP BY II.
   THE NO VAPIABLES TO BE PREDICTED ARE DENOTED BY FIRST SUBRSCRIPTS
   THROUGH NO IN APPAY X WHILE SUBSCRIPTS NO+1 THROUGH NP DENOTE
   THE NP-NC VARIABLES TO BE USED TO AID IN THE PREDICTION. OF COURS'
   NP MAY EOUAL NC.
      CALL RHJONS (M, S, A, S1, II, NP, MC, LG, XMN, GAM, SB, EE, DD, AB, B, BP, Q, IFOF
   AFTER THE FIRST CALL TO PHIONS, ARRAY ST IS SCANNED TO FIND THE
   THE MINIMUM VALUE OF THE AKAIME PPE PARAMETER BY SUBROUTINE
   FIRMIN. THE OPDER MODEL FOR WHICH THE MINIMUM OCCURS IS LMIN-1.
      CALL FREMIN (S1, LG, LMIN)
      DD(1, 1) = 99999
      LG = LMI N
  SUBROUTING REJONS IS CALLED AGAIN TO DETERMINE THE COVARIANCE AND
  COEFFICIENT MATRICES OF THE MVAR MODEL WITH THE MINIMUM VALUE
   OF THE AKAIKE FRE PARAMETER. DD(1,1)=99999. PREVENTS THE
(
   PECOMPUTATION OF THE LAG-SUM MATRICES GAM.
      CALL BHJONS (X,S,A,S1,II,NP,NC,LG,XMN,GAM,SB,EE,DD,AB,B,BB,Q,ITDT)
Ċ
   SUBROUTING ERRVAR IS CALLED TO COMPUTE THE PREDICTION ERROR
   MATRICES.
             UPON ENTRY ARRAY S CONTAINS THE ONE-STEP PREDICTION
۲
  EPROP COVAPIANCE MATRIX AND ARRAY A CONTAINS THE COEFFICIENT
  MATRICES. THE PREDICTION ERROR COVARIANCE MATRICES ARE
(
   W. TURNED IN ARRAY BB.
      CALL ERRVAR (A, B, S, BB, NP, LG)
      STOP
      END
```

```
SUBROUTINE RHJONS (X,S,A,S1,II, NP, NC, LG, XMN, GAM, SB, EE, DD, AB, B, BB, Q
            , ITOT)
   SUBBOUTINE RHJONS COMPUTES THE COEFFICIENT MATRICES AND DETERMINES IN
   PROPER ORDER FOR A MULTIVARIATE AUTOREGRESSIVE (MYAR) MODEL. ON THE
   FIRST CALL TO RHJONS, MP TIME SERIES EACH OF LENGTH II ARE INPUT INTO
   ARRAY X. THE FIRST NC TIME SERIES ARE THOSE TO BE PREDICTED. LG-1 IS
   THE MAXIMUM ORDER MVAR PROCESS TO BE FITTED TO THE DATA. THE MEAN OF
   EACH TIME SERIES IS COMPUTED AND STORED IN XMN. THE AKAIKE PPE ARE
   COMPUTED AND STORED IN S1. AFTER THE FIRST CALL, S1 IS SEARCHED FOR
C
   ITS MINIMUM VALUE AND THE INDEX OF THAT VALUE. ON THE SECOND CALL TO
   RHJONS, DD (1, 1) IS SET TO 99999.. AND LG IS SET TO THE INDEX OF THE
C
C
   HINIMUM VALUE IN S1. AFTER THE SECOND CALL THE COEPPICIENT MATRICES
С
   FOR THE LG-1 ORDER MVAR PROCESS ARE A (NP, NP, 2), A (NP, NP, 3), .
   A (NP, NP, LG). THE ONE STEP PREDICTION COVARIANCE MATRIX IS S.
      DIMENSION GAM (NP, NP, LG), A (NP, NP, LG), AB (NP, NP, LG), B (NP, NP, LG)
      DIMENSION BB(NP,NP,LG)
      DIMENSION X (NP, II), XMN (NP), S (NP, NP), SB(NP, NP), EE(NP, NP), DD (NP, NP)
      DIMENSION Q(NC,NC), S1(LG), ITOT(NP,NP)
      DIMENSION WORK (1000)
      XII=II
C WHEN DD(1, 1) EQUALS 99999. THE LAG-SUM MATRICES GAM NEED NOT
C BE COMPUTED. MISSING OR BAD DATA IN ARRAY X IS DENOTED
   BY THE VALUE OF -100.
      IF (DD (1, 1) . EQ . 99399.) GO TO 123
      DO 1900 I=1,NP
      XMN(I) = 0.
      ITOT(I,1)=0
      DO 1900 J=1,II
      IP(X(I, J).EQ.-100.) GO TO 1900
      ITOT (I, 1) = ITOT (I, 1) + 1
      XMN(I) = XMN(I) + X(I,J)
 1900 CONTINUE
      DO 1901 I=1,NP
      XMN(I) = XHN(I) / ITOT(I, 1)
      DO 1901 J=1,II
      IF (X (I, J) . EQ. - 100.) GO TO 1901
      X(I,J) = X(I,J) - XMN(I)
 1901 CONTINUE
      DO 100 I=1.NP
      DO 100 J=1, NP
      DO 100 K=1,LG
  100 GAM (I,J,K) = 0.
      DO 61 L=1, LG
      DO 61 I=1, NP
      DO 61 J=1, NP
      ITOT (I, J) = 0
      DO 62 K=L,II
      K1=K-L+1
      IF(X(I,K).EQ.-100..OR.X(J,K1).EQ.-100.) GO TO 62
      ITOT(I, J) = ITOT(I, J) + 1
      GAM(I,J,L) = GAM(I,J,L) + X(I,K) + X(J,K1)
   62 CONTINUE
      GAH (I,J,L) = GAH(I,J,L) + (II-L+1) / ITOT(I,J)
   61 CONTINUE
  123 CONTINUE
      DO 17 I=1, NP
      DO 17 J=1, NP
      A(I,J,1) = 0.
      B(I,J,1)=0.
```

```
AB (1, J, 1) = 0.
   BB (I, J, 1) = 0.
17 CONTINUE
   DO 7 1=1, NP
   B(I,I,1)=1.
   A(I, I, 1) = 1.
   BP(I, I, 1) = 1.
   AB (I,I,1)=1.
   DO 7 J=1,NP
   S(I,J) = GAM(I,J,1)
   SB(I,J) = S(I,J)
 7 CONTINUE
   IF ( LG .LE. 1 ) GO TO 124
   DO 8 L= 2. LG
   NL=1-1
   IF (NC. RQ. NP) GO TO 20
   DO 21 I=1,NC
   no 21 J=1, NC
21 ((I,J) = S(I,J)
   CALL MATINY (Q, NC, DET)
   S 1 (NI.) = DET
20 CONTINUE
   CALL MATINY (S, NP, DET)
   IF(NC.NE.NP) GO TO 22
   S1 (NL) = DET
22 CONTINUE
   CALL MATINY (SB, NT, DET)
   DO 9 I=1, MP
   DO 9 J=1, ND
   DD(I,J) = 0.
   EE(I,J) = 0.
   DO 9 K=1, NL
   K1=L-K+1
   DO 9 I1=1, NF
   EE(I, J) = EE(I, J) - BB(I, I1, K) * GAM(J, I1, K1)
   DD(I,J) = DD(I,J) - B(I,I1,Y) = GAH(I1,J,K1)
 4 CONTINUE
   DO 11 J=1, NF
   DO 11 J=1, NP
   A(I,J,L)=0.
   AB(I,J,L) = 0.
   DO 11 K=1, NP
   A(I,J,L) = A(I,J,L) + DD(I,K) * SB(K,J)
11 AB(I.J.L) = AB(I.J.L) + EE(I.K) + S(K.J)
   IF (L.EQ.2) GO TO 12
   DO 13 K=2, NL
   KN=L-R+ 1
   DO 13 I=1, NP
   DO 13 J=1, NP
   A(I,J,K) = B(I,J,K)
   AB(I,J,K) = BB(I,J,K)
   DO 13 K 1= 1, NP
   A(I,J,K) = A(I,J,K) + A(I,K1,L) + BB(K1,J,KN)
13 AB(I,J,K) = AB(I,J,K) + AB(I,K1,L) + B(K1,J,KN)
12 CONTINUE
   DO 14 I=1, NP
   DO 14 J=1, NP
   DO 14 K=1, L
   B(I,J,K) = A(I,J,K)
14 BB (I,J,K) = AB(I,J,K)
```

```
DO 15 I=1, NP
     DO 15 J=1, NP
     S(I_J) = GAM(I_J_1)
     SB(I,J) = GAM(I,J,1)
     DO 15 K=2,L
     DO 15 K1=1, NP
     S(I,J) = S(I,J) + A(I,K1,K) * GAM(J,K1,K)
  15 SB (I,J) = SB(I,J) + AB(I,K1,K) * GAM(K1,J,K)
   8 CONTINUE
124
     CONTINUE
     DO 778 I=1, NC
     DO 778 J=1,NC
778 Q(I,J) = S(I,J)
     CALL MATINY (Q, NC, DET)
     S1(LG) = DET
     WRITE (6,1800) 51
     DO 200 I=1, LG
     P1=II+(I-1) *NP+1
     F2=II-(I-1)*NP-1
F12=(F1/F2)**NC
 200 S1(I) = S1(I) *F12
     SP = S1 (1)
     DO 201 I=1,LG
201 S1(I) = S1(I) / SF
     WRITE (6,1800) S1
1800 FORMAT (2X, 'S1', 10E12.4)
     DO 77 I=1,LG
     IF(S1(I).LE.0.) S1(I)=1.
  77 S1(I) = ALOG 10(S1(I))
     PN=II-(LG-1)*NP-1
     DO 78 I=1.NP
     DO 78 J=1,NP
  78 S(I,J) = S(I,J) / FN
     RETURN
     END
```

```
DISTO TINE PREMER (S1, LG, LMIN)
   INTO SIEPBULINE SEASCHES THE VALUES OF THE AKAIKE PPE PARAMETERS
   CONTAINED IN ARRAY S1. THE MINIMUM IS FOUND AND THE ARRAY
   CONTINUE IS DESCRIBED BY LMIN. THIS CORRESPONDS TO AN MYAR MODES
   ORDER OF LMIN- 1.
      DIMENSION S1 (LG)
      SMIN= 1. E50
      00 1 T=1,LG
      IF(S^*(I),GT,SMIN) GO TO 1
      LMIN=I
      3M1 N 31 (I)
    a conflat.
      ERITI (C.S. LNIN, SI(LNIN)
    5 FORMAT (2x, LHEN, POEMIN', 15, E13.5)
      6 FORMAY (5X, 5E13.5)
      RETUIN
      END
Ţ
      SUBROUTINE MATINY (A, M, DET)
   THIS SUBROUTINE COMPUTES THE INVERSE MATRIX OF M BY M MATRIX
   A AND RETURNS THE INVERSE IN A. THE DETERMINANT OF A IS
   RETURNED IN DET.
      (R. f) A RUIcalda
      DET= 1.0
      DO 1 J-1, M
      PVT - 2 (3,3)
      DEI=DUI *PVI
      A(J,J = 1.0
      DO 2 K= 1, M
    2 A (J, K) = A (J, K' / EVT
      ως 1 π. 1,6
1Σ (π ω) 3,1,3
    3 T=A(K,J)
      A (Z, 3) = 0.0
      DO 4 L= 1. M
    4 A(K,L) = 2(K,L) - (A(J,L) *T)
    I CONTINUE
      RETURN
      END
```

```
THIS PIGGRAN IS USED TO MAKE 3, 6, 9, AND 12 HOUR MVAR FORECASTS
AND THEN COMPUTE THE 80% CONFIDENCE INTERVALS TO BE PLACED ABOUT
THIM AND COMPARE THE FORECASTS WITH THE ACTUAL CESERVATIONS VALID
AT THE FOFECAST TIME.
    DIMENSION XMM (7), A (7,7,10), ADD (7,7), YDAT (7,13), DRD (7),
         LLAT (7,4), XDAT (7,9), V (7,7), VV (7,7,10), E (7,7,10),
         FH1 (7,4), FLC (7,4), XTOMN (7), XHEAN (7,8), XMCMN (7,12)
    DIMENSION IVARN (28) , ISTAN (21)
                                    AH NEHH, MEEBH,
    DAIA ISTAN/4HHANN,4HOVER,4H
     - 4HBCIZ, 4HENBU, 4HRG - , 4HPRAU, 4HNSCH, 4HREIG, 4HMAGD,
                  . A HWEEN, 4HIGER, 4HOLE , 4HAEIS, 4HSEN , 4H
     →HEBUR,→HG
   DATA IVARN /4H1ST ,4HCLD ,4HLAYE,4HR HT,4HCEIL,4HING ,
                                                , 4 11
   1
      48HT ,48
                   ,4HTFMP,4HERAT,4HURE ,4A
            ,48
                                                 ,460-WI,4HND
                    ,4HVISI,4HEILI,4HTY ,4A
            , 4H
                    AHV-WI,4HND ,4H
                                         ,4H
KVAR IS THE VARIABLE NUMBER...1=HEIGHT OF FIRST CICUD LAYEF,
2=CLILING HIIGHT, 3=TEMPERATURE, 5=VISIBILITY, 6=U-WIND, AND
7=V-WIND. NP IS THE NUMBER OF PREDICTOR VARIABLES. LG IS THE
ORDER OF THE MVAR MCDEL PLUS ONE. THUS, FOR A 9TH CRDER MODEL
LG WOULD EQUAL 10.
    READ (5, 201) KVAR, NP, IG
201 FORMAT(1018)
   LGM1=LG-1
    LGM2=LG-2
    LGP3=LG+3
THE MEAN VECTOR, ONE-STEP PREDICTION ERROR COVARIANCE MATRIX,
AND THE COEFFICIENT MATRICES FOR THE MVAR MODEL AFE READ IN
HERE. THE SAMPLE MEAN VECTOR, WHICH IS DEFFRHINED AND REMOVED
BEFORE THE LAG-SUM MATRICES ARE COMPUTED, IS FEAR INTO ARRAY
 MMR. THE COVARIANCE MATRIX IS READ INTO ARRAY V AND THE
COEFFICIENT MATRICES ARE READ INTO AFRAY ARD AND THEN PLACED
IN ARRAY A. A(I,J,1) WILL ALWAYS BE THE IDENTITY MATRIX WHILE
COEFFICIENT MAIRICES A1, A2, A3, ... WILL BE PLACED IN A (I, J, 2),
A(I,J,3),A(I,J,4),...,RESPECTIVELY.
    READ (5,200) XMN
200 FURMAT (7F11.5)
    \text{READ}(5,290) = (\{V(I,J),J=1,7\},I=1,7)
    DO 5 L=1, LG
    PEAD(5, 200) (ARD(I,J),J=1,7),I=1,7)
    DC 5 I=1,NP
    DO 5 J=1,NP
  5 A(I,J,L) = ARD(I,J)
 IF THE VARIABLE IS TEMPERATURE, THE GRAND MEANS, HOWELY MEANS
 AND MONIBLY MEANS WHICH WERE REMOVED BEFORE THE MVAR MODEL
 WAS DETERMINED, MUST BE READ IN HERE SO THAT THEY MAY BE
 ADDED EACK TO THE FORECAST VALUES.
    IF (KVAR.NE.3) GO TO 110
    READ (5, 101) XTCMN
    READ(5, 101) = ((XHEMN(I,J),I=1,7),J=1,8)
    READ (5, 101) ((XMCMN(I,J), I=1,7), J=1,12)
101 FORMAT (7F8.3)
110 CONTINUE
    CALL EBRVAR (A, E, V, VV, NP, LG)
THE OBSERVATIONS TO BE USED TO MAKE AND VARIFY THE FORECASTS
 ARE REAL IN HEFE. IT IS ASSUMED THAT THE CONTRIBUTION OF
 THE HOURLY AND MONTHLY MEANS HAVE BEEN REMOVED BEFORE THE
 TEMPERATURE DATA HAS BEEN READ IN AND THAT TRANSFORMED
 VISIBILITY AND CLOUD HEIGHT VARIABLES ARE TO BE FEAD IN.
 ARTAY YUAT IS DIMENSIONED NP BY LG+3.
                                        THE CBSERVATION TO
```

```
be IMIABED WITH THE 12-HOUP FORECAST IS CONTAINED IN ELEMFRIT
 TRAL (I, 1), THE OBSERVATION VALID AT THE ZERO FORECAST TIME
 IS CONTAINED IN YOAT (1,5), AND THE OBSERVATION FABILEST IN
    FASI IS CONTAINED IN YDAT (I, LG+3).
    5251(5,200) = ((YDAT(I,J),I=1,NF),J=1,LGP3)
    DO 10 I=1,NE
    30 10 3=1,13m1
 10 17AT (I, J) = YDAT (I, J+4) - XMN (I)
    DC 20 IFCST=1,4
    If (IFOST, EQ. 1) GO TO 21
    DU 22 I=1,NF
DO 23 3=1,LGM2
 23 NDAT (1, LG-J) = NDAT (1, 1GM1-J)
    SUNTINUE
    30 40 I≠1,NE
    LOAT (I, IFUST) -1.
    00 25 L=1,LGM1
    100 25 J=1,NI
 25 FDAI(1, IFSST) = FDAT(1, IFCST) - A(1, J, L+1) * XDAT(J, I)
 20 CONTINGI
    IF (KVAN.NE.3) GC TO 210
 THE HOUS AND MONTH OF THE FORTCASI ZERO LIME ASE SEAD IN
 HELL ONLY YOR LEMPERATURE SO THAT THE MONTHLY AND HOURLY
 TEAND CAN BE ADDED BACK IN. IMPRET FOR DOZ, IMAREZ FOR DOZ.
 ..., IHET -5 FOR 212. IMCF=1 FOR JANUARY AND IMOF=12 FOR
 DECEMBER.
    TEAL (5, 201) IHRF, INOF
    DO 211 I=1,NP
    DO 211 J=1,4
    IBS=IHPF+J
    IF (IND. GT. 5) IHR=IHP-9
    IMC-IMIE
    (I, J) = FDAT (I, J) + XHRMN (I, IHE) + XHCMN (I, IMO) - XTOMN (I)
IDAI(I, 5-J) = YDAI(I, 5-J) + NHRMN (I, IHR) + NHCMN (I, IMG) - XIOMN (I)

LII CONTINUE
217 :077 :39 E
    30 30 I=1, WP
30 30 J=1, W
    FDAT (I,J) FPEAT (I,J) + XMN(I)
    SDESLAT (VV (I,I,J))
    INI(I,J) = FDAT(I,J) + 1.28 * SD
    rLC(I,3) = FDAT(I,3) - 1.28 * SD
    ICHE = EVAF
    IF (IUNE.GT. 2. AND. ICHK.NE.5) GO TO 30
    AFULT-1000.
    IF (ICUE.Ig.5) XMULT=2000.
    IF (FOAT (I,J), LE.O.) FDAT (I,J) = 1.E+13
    IF (FHI (I, J) . LL.(.) FHI (I, J) = 1. E-13
    IF (FLO(I,J).LE.O.) FLO(I,J) = 1.E-13
    FUAT (I,J) = - MMULT * ALOG (FDAT (I,J))
    XLC=FLC (1,J)
    XdI=FHI(I,J)
    FHI (I, J) = -XMULT * ALOG (XLO)
    FLO(I,J) = -XMULT * ALOG(XHI)
    IF (FLO(I,J).LI.O.) FLO(I,J)=O.
    iDAT(x,5-J) = -XMULT * ALCG(YDAT(I,5-J))
 30 CONTINUE
    KV 1 = (KVAF - 1) * 4 + 1
```

```
SUBNOUTING ERRVAR (A, B, V, VV, NP, LJ)
  DIMERSION V(NP, NP), A (NP, NP, LG), B (NP, NP, LG), VV (NF, NP, LG)
  00 1 I=1, NP
   DO 1 J=1, NP
1 \ VV(I,J,1) = V(I,J)
   LGM1=LG-1
  DO \epsilon L=1,LGM1
   DO 6 I=1, NP
   DO 6 J=1,NP
  DG & LK=1,L
   IF (LK.GT.1) GO TO 7
   E(I,J,L) = -A(I,J,L+1)
   GO IU U
7 CONTINUE
   DO B KK=1, NP
 8 8 (I,J,L) = B(I,J,L) - B(I,KK,LK-1) * A(KK,J,LK)
 o CONTINUE
   DO 10 L=2, LG
   DO 10 I=1,NP
   DO 10 J=1, NP
   VV(I,J,L) = VV(I,J,L-1)
   DO 10 KK=1,NP
   DO 16 LL=1, KP
10 VV (I,J,L) = VV (I,J,L) +B (I,KK,L-1) +VV (KK,LL,1) +B (J,LL,L-1)
   RETURN
   E \times D
```

#### FLOWCHART OF ANALYSIS PROCEDURE

#### Initialization

Before any subroutine calls: II is the number of NP-dimensional observation vectors an MVAR model is to be found for, the maximum order model to be tried is LG-1, the array X dimensioned NP by II contains the observation vectors.

#### 1st Call of Subroutine RHJONS

MVAR models of order zero to order LG are fitted to the II No-dimensional observation vectors. The values of the Akaike TRE parameter are stored in array S1.

#### Call Subroutine FPEMIN

Array S1 is searched for the minimum value of the FPE parameter. Array element LMIN denotes the minimum and LMIN-1 is the order of the MVAR model.

### 2nd Call of Subroutine RHJONS

An MVAR model of order LMIN-1 is fitted to the II NP-dimensional observation vectors. The one-step prediction error covariance matrix is contained in array S and the coefficient matrices in array A.

#### Call Subroutine ERRVAR

Prediction error covariance matrices for various step forecasts are computed and contained in array BB.

